

underground mining.





We are happy to recommend Bridon-Bekaert as a reputable manufacturer and supplier of wire ropes in challenging key application areas. We use their wire ropes on our key equipment and the uptime is very essential for us as a successful mining operator. Bridon-Bekaert also provides excellent training to our maintenance personnel on key aspects of wire rope usage and maintenance.

Bridon brand products have stood up to our expectations from a world class wire rope manufacturer.

ropes.

As a leading innovator, developer and producer of the best performing ropes and advanced cords globally, the Group provides superior value solutions to the oil & gas, mining, crane, elevator and other industrial sectors.

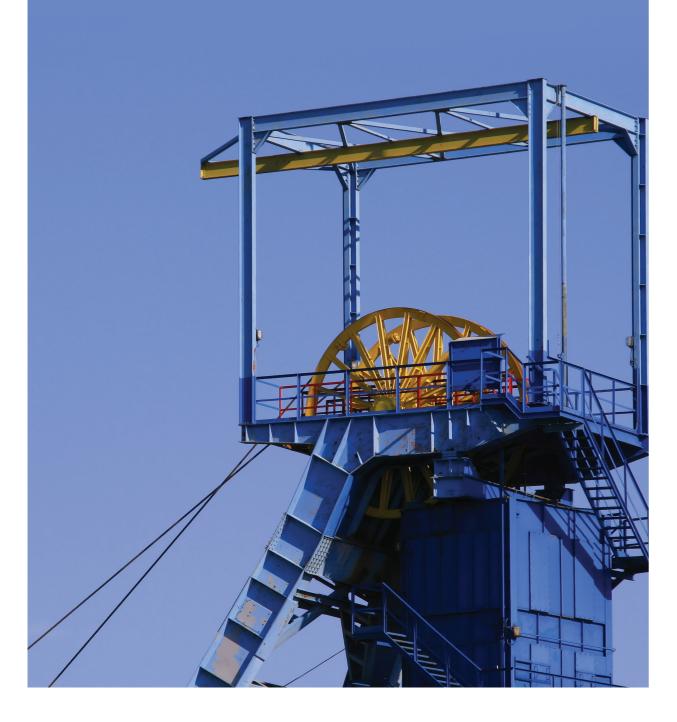
Two of the most enduring wire and rope pioneers joined forces in 2016 to make this ambition real. Bridon-Bekaert Ropes Group has a global manufacturing footprint and employs approximately 2500 people worldwide.

Drawing from a background of long standing experience and technology, Bridon-Bekaert ropes and services meet and exceed the demands of the mining industry.

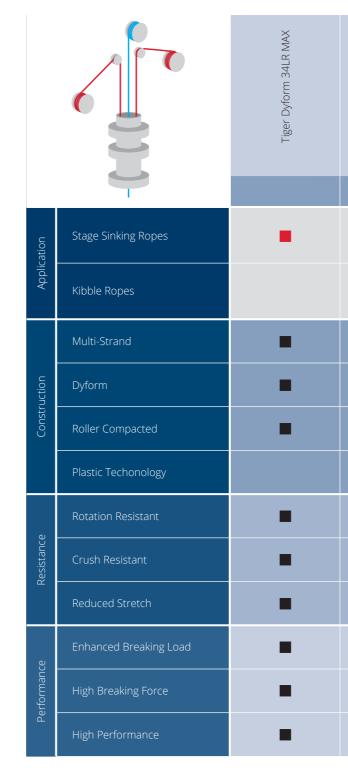
BRIDON · BEKAERT

Bridon-Bekaert Ropes Group is the world's premier supplier of mission-critical advanced cords, steel wire ropes, and fibre synthetic

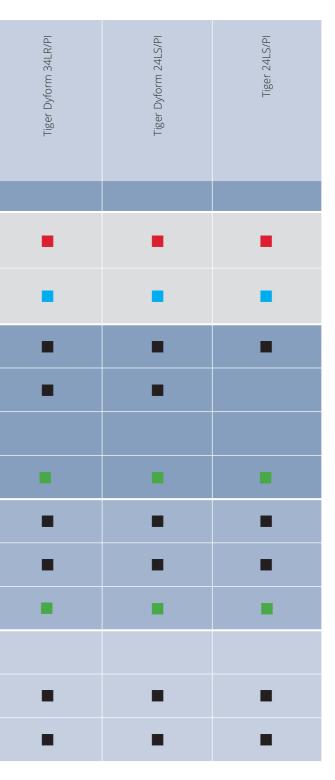
product selection.



Stage Sinking Ropes



Applies to PI products only.



Hoist Ropes

Parallel Drum Hoist

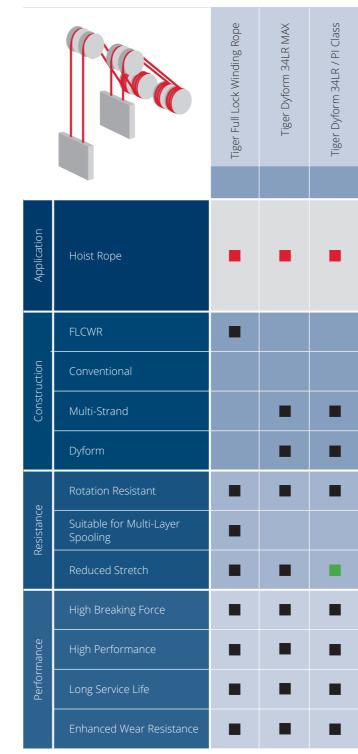
		Tiger Full Lock Winding Rope	Tiger Dyform 34LR MAX	Tiger Dyform 34LR / PI Class	Tiger Dyform 24LS/PI	Tiger 24LS/PI	Tiger Dyform 18M/PI	Tiger 6T Compound / Bristar	Tiger Dyform 6R	Tiger 6R
Application	Hoist Rope	•	•	•	•	•	•	•	•	•
	FLCWR									
uction .	Conventional									-
Construction	Multi-Strand						•			
-	Dyform		•				•			
	Rotation Resistant									
Resistance	Suitable for Multi-Layer Spooling									
. K	Reduced Stretch		•							
	High Breaking Force									
nance	High Performance	•	•		•					
Performance	Long Service Life									
	Enhanced Wear Resistance	•	•	•	•		•		•	

Applies to PI products only.

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Hoist Ropes

Blair Hoist



Applies to PI products only.

Tiger Dyform 24LS/PI	Tiger 24LS/PI	Tiger Dyform 18M/P1	Tiger 6T Compound / Bristar	Tiger Dyform 6R	Tiger 6R
•	-	-	-	•	-
		•			
•				•	
			•	•	
•		•		•	
•	•	•	•	•	
•	•	•	•	•	•
•		•	•	•	

Hoist and Balance Ropes

Ground Mounted Friction Hoist

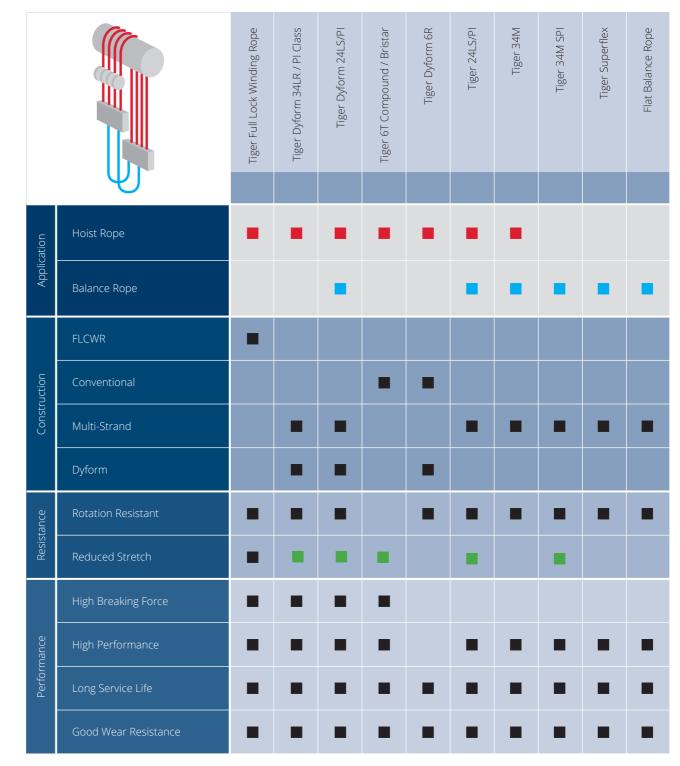
		Tiger Full Lock Winding Rope	Tiger Dyform 34LR / PI Class	Tiger Dyform 24LS/PI	Tiger 6T Compound / Bristar	Tiger Dyform 6R	Tiger 34M SPI	Tiger 24LS/PI	Tiger 34M	Tiger Superflex	Flat Balance Rope
ation	Hoist Rope	•	-	-	•	•		•	•		
Application	Balance Rope			•			•	•	•	•	•
	FLCWR										
uction	Conventional				•	•					
Construction	Multi-Strand		-	•			•	•	-	-	•
	Dyform	•	-	-		•					
ance	Rotation Resistant		-	-			•	•	-		•
Resistance	Reduced Stretch	•									
	High Breaking Force										
Jance	High Performance		-	•	•		•	•			•
Performance	Long Service Life	•		•	•	•	•	•	•	•	•
	Good Wear Resistance					•					-

Applies to PI products only.

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Hoist and Balance Ropes

Tower Mounted Friction Hoist with Deflectors

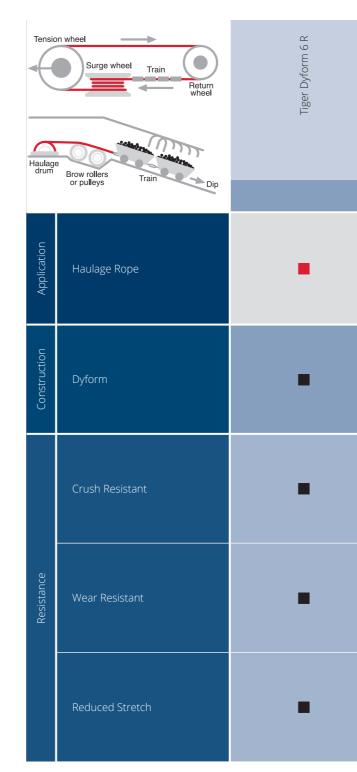


Applies to PI products only.

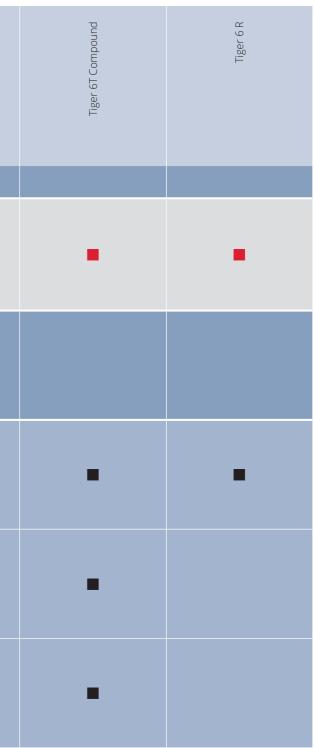
Guide & Rubbing Ropes

		Tiger Half Lock Guide Rope
Application	Guide & Rubbing Rope	
	Spiral Construction	-
	Corrosion Resistant	
Resistance	Wear Resistant	
	Reduced Stretch	
	High Performance	
Performance	Long Service Life	
	Decreased Downtime	

Haulage Ropes



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Conveyor Drive Rope (CDR)

_	Gocco Cocco Co	Zebra	Dyform Bristar	Tiger Dyform 6 CDR	Tiger 6 CDR
Application	Rope Driven Conveyor (RDC)	•	•	•	•
Construction	Dyform / Compacted	•	•	•	
Constr	Plastic Technology		•		
	Wear Resistant				
Resistance	Reduced Vibration and Noise	•			
	Reduced Stretch		•		
41	High Performance			•	
Performance	Long Life		•	•	
- u -	Decreased Downtime	•	•	•	•

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product tables.



Tiger Dyform 34LR MAX

Sinking Stage Hoist Rope

Lay I	ype	Lay Dir	rection	Fin	ish		Core	
Ord	Langs	Right Hand	Left Hand	Bright	Galv	NFC	SFC	WSC
•	•	•	•	•	•			•
		Lay Type Ord Langs • •						

Nominal	Naminal Longth Mass	Calculated Minimu	um Breaking Force
Diameter	Nominal Length Mass	Grade 2060 N/mm ²	Grade 2160 N/mm ²
mm	kg/m	kN	kN
34	6.32	1128	1187
36	7.12	1274	1334
38	7.95	1422	1491
40	8.82	1579	1648
42	9.73	1717	1795
44	10.69	1913	1952
44.5	10.95	1952	2001
46	11.65	2080	2139
47.6	12.51	2237	2286
48	12.73	2276	2325
50	13.76	2462	2521
50.8	14.23	2541	2590
52	14.88	2659	2747

The nominal length mass values are for fully lubricated ropes.



Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.



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Tiger Hoist Roj	Dyfo	rm 34	1LR/P				
Lay 1	Гуре	Lay Di	rection	Fin	Core		
Ord	Langs	Right Hand	Left Hand	Bright	Galv	WSC	
•	•	•	•	•	•	•	

.	Approx		Calculated	d Aggregate E	Breaking Forc	e	(Calculated Mi	nimum Break	king Force	
Diameter	Approx Mass	1570 N/ mm ²	1770 N/ mm ²	1860 N/ mm ²	1960 N/ mm²	2160 N/ mm ²	1570 N/ mm ²	1770 N/ mm ²	1860 N/ mm ²	1960 N/ mm ²	2160 N/ mm ²
mm	kg/m	kN	kN	kN	kN	kN	kN	kN	kN	kN	kN
19	1.82	322	364	382	403	444	248	280	294	310	342
20	2.02	357	403	423	446	492	275	310	326	343	379
21	2.22	394	444	467	492	542	303	342	359	379	417
22	2.44	432	488	512	540	595	333	375	394	416	458
23	2.67	473	533	560	590	650	364	410	431	454	501
24	2.90	515	580	610	643	708	396	447	469	495	545
25	3.15	559	630	662	697	769	430	485	509	537	592
26	3.41	604	681	716	754	831	465	524	551	581	640
27	3.68	652	735	772	814	897	502	566	594	626	690
28	3.96	701	790	830	875	964	539	608	639	674	742
29	4.24	752	848	891	939	1030	579	652	686	723	796
30	4.54	804	907	953	1000	1100	619	698	734	773	852
31	4.85	859	969	1010	1070	1180	661	746	784	826	910
32	5.17	915	1030	1080	1140	1260	705	795	835	880	970
33	5.49	974	1090	1150	1210	1340	750	845	888	936	1030
34	5.83	1030	1160	1220	1290	1420	796	897	943	993	1090
35	6.18	1090	1230	1290	1360	1500	843	951	999	1050	1160
36	6.54	1150	1300	1370	1440	1590	892	1000	1050	1110	1220
37	6.91	1220	1380	1450	1520	1680	942	1060	1110	1170	1290
38	7.28	1290	1450	1530	1610	1770	994	1120	1170	1240	1360
39	7.67	1360	1530	1610	1690	1870	1040	1180	1240	1300	1440
40	8.08	1430	1610	1690	1780	1960	1100	1240	1300	1370	1510
41	8.50	1480	1670	1760	1850	2040	1140	1280	1350	1420	1570
42	8.92	1550	1750	1840	1940	2140	1200	1350	1420	1490	1650
43	9.35	1630	1840	1930	2040	2240	1250	1410	1490	1570	1730
44	9.79	1710	1920	2020	2130	2350	1310	1480	1560	1640	1810
45	10.2	1790	2010	2120	2230	2460	1370	1550	1630	1720	1890
46	10.7	1870	2100	2210	2330	2570	1440	1620	1700	1790	1980
47	11.2	1950	2200	2310	2430	2680	1500	1690	1780	1870	2060
48 49	11.6	2030	2290	2410	2540	2800	1560	1760	1850	1950	2150
49 50	12.1	2120	2390	2510	2640	2920	1630	1840	1930	2040	2240
50	12.6 13.2	2210 2290	2490 2590	2610 2720	2750 2870	3040 3160	1700 1770	1910 1990	2010 2090	2120 2210	2340
51	13.2	2290	2690	2720	2870	3160	1840	2070	2090	2210	2430 2530
53	14.2	2390	2790	2030	3090	3280	1910	2070	2160	2380	2630
54	14.7	2570	2900	3050	3210	3540	1980	2230	2350	2300	2030
55	15.3	2670	3010	3160	3330	3670	2050	2320	2430	2570	2830
56	15.9	2770	3120	3280	3460	3810	2030	2400	2430	2660	2830
57	16.4	2870	3230	3400	3580	3950	2210	2490	2620	2760	3040
58	17.0	2970	3350	3520	3710	4090	2280	2580	2710	2850	3150
59	17.6	3070	3460	3640	3840	4090	2360	2670	2800	2950	3250
60	18.2	3180	3580	3770	3970	4230	2450	2760	2900	3050	3370
61	18.8	3280	3700	3890	4100	4520	2530	2850	3000	3160	3480
62	19.4	3390	3830	4020	4240	4670	2610	2940	3090	3260	3590
63	20.1	3500	3950	4150	4380	1070	2700	3040	3200	3370	5550
64	20.7	3620	4080	4280	4520		2780	3140	3300	3480	
65	21.4	3730	4210	4420	4660		2870	3240	3400	3590	

The nominal length mass values are for fully lubricated ropes.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.



Tiger 24 LS PI Hoist Rope • • • • •

			Calculated	Aggregate Bre	aking Force			Calculated	Minimum Bre	aking Force	2060 N/mm ² kN 451 490 530 571 614 659 705 753 803 854 906 960 1010 1070 1130 1190 1250		
Nominal Diameter	Approx. Mass	1570 N/mm²	1770 N/mm²	1860 N/mm²	1960 N/mm²	2060 N/mm²	1570 N/mm²	1770 N/mm²	1860 N/mm²	1960 N/mm²	2060 N/mm²		
mm	kg/m	kN											
24	2.55	441	497	523	551	579	344	388	407	429	451		
25	2.77	479	540	567	598	628	373	421	442	466	490		
26	3.00	518	584	613	646	679	404	455	478	504	530		
27	3.23	558	629	661	697	733	435	491	516	544	571		
28	3.47	600	677	711	750	788	468	528	555	585	614		
29	3.72	644	726	763	804	845	502	566	595	627	659		
30	3.98	689	777	817	861	905	538	606	637	671			
31	4.25	736	830	872	919	966	574	647	680	717	753		
32	4.54	784	884	929	979	1020	612	690	725	764			
33	4.82	834	940	988	1040	1090	651	733	771	812			
34	5.11	885	998	1040	1100	1160	691	779	818	862			
35	5.42	938	1050	1110	1170	1230	732	825	867	914			
36	5.73	993	1110	1170	1240	1300	774	873	917	967			
37	6.06	1040	1180	1240	1300	1370	818	922	969	1020			
38	6.39	1100	1240	1310	1380	1450	863	973	1020	1070			
39	6.73	1160	1310	1380	1450	1520 1600	909	1020	1070	1130			
40	7.08	1220	1380	1450	1530	1600	956	1070	1130	1190			
41 42	7.44 7.81	1280 1350	1450 1520	1520 1600	1600 1680	1770	1000 1050	1130 1180	1190 1240	1250 1310	1310 1380		
42	8.18	1330	1520	1670	1760	1850	1100	1240	1240	1370	1450		
44	8.57	1480	1670	1750	1850	1940	1150	1300	1370	1440	1510		
45	8.96	1550	1740	1830	1930	2030	1210	1360	1430	1510	1580		
46	9.37	1620	1820	1920	2020	2120	1260	1420	1490	1570	1650		
47	9.78	1690	1900	2000	2110	2220	1320	1480	1560	1640	1730		
48	10.20	1760	1990	2090	2200	2310	1370	1550	1630	1710	1800		
49	10.60	1840	2070	2180	2290	2410	1430	1610	1700	1790	1880		
50	11.10	1910	2160	2260	2390	2510	1490	1680	1770	1860	1960		
51	11.50	1990	2240	2360	2480	2610	1550	1750	1840	1940	2040		
52	12.00	2070	2330	2450	2580	2710	1610	1820	1910	2010	2120		
53	12.40	2150	2420	2550	2680	2820	1670	1890	1980	2090	2200		
54	12.90	2230	2510	2640	2790	2930	1740	1960	2060	2170	2280		
55	13.40	2310	2610	2740	2890	3040	1800	2030	2140	2250	2370		
56	13.90	2400	2700	2840	3000	3150	1870	2110	2220	2340	2450		
57	14.40	2490	2800	2950	3100	3260	1940	2180	2300	2420	2540		
58	14.90	2570	2900	3050	3210	3380	2010	2260	2380	2510	2630		
59	15.40	2660	3000	3160	3330	3500	2080	2340	2460	2590	2730		
60	15.90	2750	3110	3260	3440	3620	2150	2420	2540	2680	2820		
61	16.50	2850	3210	3370	3560	3740	2220	2500	2630	2770	2910		
62	17.00	2940	3320	3490	3670	3860	2290	2590	2720	2860	3010		
63	17.60	3040	3420	3600	3790	3990 4110	2370	2670	2810	2960	3110		
64	18.10	3130	3530	3710	3910		2440	2760	2900	3050	3210		
65	18.70	3230	3650	3830	4040	4240	2520	2840	2990	3150	3310		

The nominal length mass values are for fully lubricated ropes.

Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.



Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product. Read cautionary notice - Restrictions on the use of large diameter multi-strand ropes.



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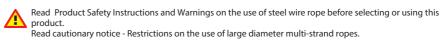
Tiger 24 LS

Hoist Rope

	Lay Type			Lay Directio	n		Finish			Core	
Ord		Langs	Rig	ht	Hand	Brigh	t	Galv	NFC		SFC
		•	•	,	•	•		•	•		•
			Calculated	Aggregate Bre	aking Force			Calculated	Minimum Bre	aking Force	
Nominal Diameter	Approx. Mass	1570 N/mm²	1770 N/mm²	1860 N/mm²	1960 N/mm²	2060 N/mm²	1570 N/mm²	1770 N/mm²	1860 N/mm²	1960 N/mm²	2060 N/mm²
mm	kg/m	kN									
24	2.51	442	499	524	552	581	345	389	409	431	453
25	2.73	480	541	569	599	630	374	422	444	467	491
26	2.95	519	585	615	648	681	405	457	480	506	531
27	3.18	560	631	663	699	735	437	492	517	545	573
28	3.42	602	679	714	752	790	470	530	556	586	616
29	3.67	646	728	765	807	848	504	568	597	629	661
30	3.92	691	780	819	863	907	539	608	639	673	708
31	4.19	738	832	875	922	969	576	649	682	719	756
32	4.47	787	887	932	982	1030	614	692	727	766	805
33	4.75	837	943	991	1040	1090	653	736	773	815	856
34	5.05	888	1000	1050	1100	1160	693	781	821	865	909
35	5.35	941	1060	1110	1170	1230	734	828	870	917	963
36	5.65	996	1120	1180	1240	1300	777	876	920	970	1010
37	5.97	1050	1180	1240	1310	1380	820	925	972	1020	1070
38	6.30	1110	1250	1310	1380	1450	865	976	1020	1080	1130
39	6.64	1160	1310	1380	1450	1530	912	1020	1080	1130	1190
40	6.98	1230	1380	1450	1530	1610	959	1080	1130	1190	1250
41	7.33	1290	1450	1530	1610	1690	1000	1130	1190	1250	1320
42	7.69	1350	1520	1600	1690	1770	1050	1190	1250	1320	1380
43	8.08	1420	1600	1680	1770	1860	1100	1250	1310	1380	1450
44	8.45	1480	1670	1760	1850	1950	1160	1300	1370	1440	1520
45	8.84	1550	1750	1840	1940	2040	1210	1360	1430	1510	1590
46	9.24	1620	1830	1920	2030	2130	1260	1430	1500	1580	1660
47	9.64	1690	1910	2010	2120	2220	1320	1490	1560	1650	1730
48	10.1	1770	1990	2090	2210	2320	1380	1550	1630	1720	1810
49	10.5	1840	2080	2180	2300	2420	1430	1620	1700	1790	1880
50	10.9	1920	2160	2270	2390	2520	1490	1690	1770	1870	1960
51	11.4	1990	2250	2360	2490	2620	1550	1750	1840	1940	2040
52	11.8	2070	2340	2460	2590	2720	1620	1820	1920	2020	2120
53	12.3	2150	2430	2550	2690	2830	1680	1890	1990	2100	2210
54	12.7	2240	2520	2650	2790	2940	1740	1970	2070	2180	2290
55	13.2	2320	2620	2750	2900	3050	1810	2040	2140	2260	2380
56	13.7	2410	2710	2850	3000	3160	1880	2120	2220	2340	2460
57	14.2	2490	2810	2950	3110	3270	1940	2190	2300	2430	2550
58	14.7	2580	2910	3060	3220	3390	2010	2270	2380	2510	2640
59	15.2	2670	3010	3170	3340	3510	2080	2350	2470	2600	2730
60	15.7	2760	3120	3270	3450	3630	2150	2430	2550	2690	2830
61	16.2	2860	3220	3380	3570	3750	2230	2510	2640	2780	2920
62	16.8	2950	3330	3500	3680	3870	2300	2590	2730	2870	3020
63	17.3	3050	3440	3610	3800	4000	2380	2680	2810	2970	3120
64	17.9	3140	3550	3730	3930	4130	2450	2760	2900	3060	3220
65	18.4	3240	3660	3840	4050	4260	2530	2850	3000	3160	3320

The nominal length mass values are for fully lubricated ropes.

Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.









Tiger Dyform 24 LS Hoist Rope Left Hand • • • • • • .

NI			Calculated A	vggregate Bre	aking Force			Calculated	Minimum Bre	aking Force	
Nominal Diameter	Approx. Mass	1570 N/mm²	1770 N/mm²	1860 N/mm²	1960 N/mm²	2060 N/mm²	1570 N/mm²	1770 N/mm²	1860 N/mm²	1960 N/mm²	2060 N/mm²
mm	kg/m	kN									
24	2.74	481	543	570	601	632	375	423	445	469	493
25	2.97	522	589	619	652	685	407	459	483	509	535
26	3.21	565	637	669	705	741	441	497	522	550	578
27	3.46	609	687	722	761	800	475	536	563	593	624
28	3.73	655	739	776	818	860	511	576	606	638	671
29 30	4.00 4.27	703 752	793 848	833 891	878 939	923 987	548 587	618 662	650	685 733	719
30	4.27	803	848 906	952	1000	1050	627	706	695 742	733	770 822
32	4.30	856	965	1010	1060	1120	668	753	742	834	876
33	5.17	910	1020	1070	1130	1190	710	801	841	887	932
34	5.49	967	1090	1140	1200	1260	754	850	893	941	989
35	5.82	1020	1150	1210	1270	1340	799	901	946	997	1040
36	6.16	1080	1220	1280	1350	1420	845	953	1000	1050	1100
37	6.50	1140	1290	1350	1420	1500	893	1000	1050	1110	1170
38	6.86	1200	1360	1430	1500	1580	942	1060	1110	1170	1230
39	7.22	1270	1430	1500	1580	1660	992	1110	1170	1230	1300
40	7.60	1330	1500	1580	1670	1750	1040	1170	1230	1300	1360
41	7.98	1400	1580	1660	1750	1840	1090	1230	1290	1360	1430
42	8.37	1470	1660	1740	1840	1930	1150	1290	1360	1430	1510
43	8.79	1540	1740	1830	1930	2020	1200	1360	1420	1500	1580
44 45	9.20 9.62	1610 1690	1820 1900	1910 2000	2020 2110	2120 2220	1260 1320	1420 1480	1490 1560	1570 1640	1650 1730
45	10.10	1770	1900	2000	2200	2320	1320	1550	1630	1720	1810
40	10.10	1840	2080	2180	2300	2420	1440	1620	1700	1720	1890
48	10.90	1920	2170	2280	2400	2520	1500	1690	1780	1870	1970
49	11.40	2000	2260	2370	2500	2630	1560	1760	1850	1950	2050
50	11.90	2090	2350	2470	2600	2740	1630	1830	1930	2030	2130
51	12.30	2170	2450	2570	2710	2850	1690	1910	2000	2110	2220
52	12.80	2260	2540	2670	2820	2960	1760	1980	2080	2200	2310
53	13.30	2340	2640	2780	2930	3080	1830	2060	2170	2280	2400
54	13.90	2430	2740	2880	3040	3190	1900	2140	2250	2370	2490
55	14.40	2520	2850	2990	3150	3310	1970	2220	2330	2460	2580
56	14.90	2620	2950	3100	3270	3440	2040	2300	2420	2550	2680
57	15.40	2710	3060	3210	3390	3560	2110	2380	2510	2640	2780
58	16.00	2810	3170	3330	3510	3690	2190	2470	2590	2730	2870
59	16.50	2910	3280	3440	3630		2270	2550	2680	2830	
60 61	17.10 17.70	3010 3110	3390 3500	3560 3680	3750 3880		2340 2420	2640 2730	2780 2870	2930 3020	
62	17.70	3210	3620	3800	4010		2420	2730	2870	3020	
63	18.80	3310	3740	3930	4010		2580	2910	3060	3230	
64	19.50	3420	3860	4050	4270		2670	3010	3160	3330	
65	20.10	3530	3980	4180	4410		2750	3100	3260	3440	

The nominal length mass values are for fully lubricated ropes. Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this Read Proc product. Read cautionary notice - Restrictions on the use of large diameter multi-strand ropes.

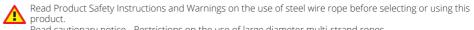


This table is for guidance purposes only with no guarantee or warranty (express or implied) as to its accuracy. The products described may be subject to change without notice, and should not be relied on without further advice from Bridon-Bekaert.

Tiger Dyform 24 LS PI Hoist Rope

	Lay Type	<u>.</u>		Lay Directio	'n		Finish	~		Core	
Ord		Langs	Righ		Hand	Brigh		Galv	NFC		SFC
									•		•
			Calculated A	Aggregate Bre	aking Force			Calculated	Minimum Bre	aking Force	
Nominal Diameter	Approx. Mass	1570	1770	1860	1960	2060	1570	1770	1860	1960	2060
Diameter	101035	N/mm²	N/mm ²								
mm	kg/m	kN	kN	kN	kN	kN	kN	kN	kN	kN	kN
24	2.76	479	540	568	598	629	374	421	443	466	490
25	3.00	520	586	616	649	682	405	457	480	506	532
26	3.24	562	634	666	702	738	438	494	520	547	575
27	3.50	606	684	718	757	796	473	533	560	590	621
28	3.76	652	735	773	814	856	509	573	603	635	667
29	4.03	700	789	829	874	918	546	615	646	681	716
30	4.31	749	844	887	935	983	584	658	692	729	766
31	4.60	800	901	947	998	1040	624	703	739	779	818
32	4.91	852	961	1000	1060	1110	664	749	787	830	872
33	5.22	906	1020	1070	1130	1180	707	797	837	882	927
34	5.53	962	1080	1140	1200	1260	750	846	889	937	984
35	5.87	1010	1140	1200	1270	1330	795	896	942	993	1040
36	6.21	1070	1210	1270	1340	1410	841	948	996	1050	1100
37	6.56	1130	1280	1350	1420	1490	888	1000	1050	1100	1160
38	6.92	1200	1350	1420	1500	1570	937	1050	1110	1170	1230
39	7.29	1260	1420	1500	1580	1660	987	1110	1170	1230	1290
40	7.66	1330	1500	1570	1660	1740	1030	1170	1230	1290	1360
41	8.05	1390	1570	1650	1740	1830	1090	1230	1290	1360	1430
42	8.46	1460	1650	1730	1830	1920	1140	1290	1350	1420	1500
43	8.86	1530	1730	1820	1920	2010	1200	1350	1420	1490	1570
44	9.27	1610	1810	1900	2010	2110	1250	1410	1480	1560	1640
45	9.70	1680	1900	1990	2100	2210	1310	1480	1550	1640	1720
46	10.10	1760	1980	2080	2190	2310	1370	1540	1620	1710	1800
47	10.60	1830	2070	2170	2290	2410	1430	1610	1690	1790	1880
48	11.00	1910	2160	2270	2390	2510	1490	1680	1770	1860	1960
49	11.50	1990	2250	2360	2490	2620	1550	1750	1840	1940	2040
50	12.00	2080	2340	2460	2590	2720	1620	1820	1920	2020	2120
51	12.50	2160	2440	2560	2700	2840	1680	1900	2000	2100	2210
52	13.00	2250	2530	2660	2800	2950	1750	1970	2070	2190	2300
53	13.50	2330	2630	2760	2910	3060	1820	2050	2160	2270	2390
54	14.00	2420	2730	2870	3020	3180	1890	2130	2240	2360	2480
55	14.50	2510	2830	2980	3140	3300	1960	2210	2320	2450	2570
56	15.00	2600	2940	3090	3250	3420	2030	2290	2410	2540	2670
57	15.60	2700	3040	3200	3370	3540	2100	2370	2490	2630	2760
58	16.10	2790	3150	3310	3490	3670	2180	2460	2580	2720	2860
59	16.70	2890	3260	3430	3610		2250	2540	2670	2820	
60	17.20	2990	3370	3540	3740		2330	2630	2760	2910	
61	17.80	3090	3490	3660	3860		2410	2720	2860	3010	
62	18.40	3190	3600	3780	3990		2490	2810	2950	3110	
63	19.00	3300	3720	3910	4120		2570	2900	3050	3210	
64	19.60	3400	3840	4030	4250		2650	2990	3140	3310	
65	20.20	3510	3960	4160	4380		2740	3090	3240	3420	
05	20.20	5510	5500	-100	-500		2740	5050	5240	5420	

The nominal length mass values are for fully lubricated ropes. Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.



Read cautionary notice - Restrictions on the use of large diameter multi-strand ropes.







Tiger 34M SPI

Balance Rope

✓ Fully Sheathed and Plastic Impregnated rope

	Lay Type			Lay Direction			Finish			Core	
Ord		Langs	Right Hai	nd L	_eft Hand	Bright		Galv	NFC	SFC	WSC
		•	•		•	•		•	•	•	
Nominal	Nominal	Calcu	lated Aggreg	ate Breaking	Force			Calculated N	/linimum Bre	aking Force	
lasticated	length	Grade	Grade	Grade	Grade	Grade	Grade	Grade	Grade	Grade	Grade
Diameter	mass	1180	1370	1570	1770	1960	1180	1370	1570	1770	1960
~~~	kg/100m	kN	kN	kN	kN	kN	kN	kN	kN	kN	kN
mm	kg/100m	KIN	KIN	KIN	KIN	KIN	KIN	KIN	KIN	KIN	KIN
30	3.92	473	549	630	710	786	355	412	472	532	590
31	4.19	505	587	672	758	840	379	440	504	568	630
32	4.46	538	625	716	808	895	404	469	537	606	671
33	4.74	573	665	762	859	951	429	499	571	644	713
34	5.04	608	706	809	912	1010	456	529	607	684	757
35	5.34	644	748	857	967	1070	483	561	643	725	803
36	5.65	682	791	907	1020	1130	511	593	680	767	849
37	5.96	720	836	958	1080	1190	540	627	718	810	897
38	6.29	759	882	1010	1130	1260	569	661	758	854	946
39	6.63	800	929	1060	1200	1320	600	696	798	900	997
40	6.98	842	977	1120	1260	1390	631	733	840	947	1040
41	7.32	884	1020	1170	1320	1460	663	770	882	995	1100
42	7.68	928	1070	1230	1390	1540	696	808	926	1040	1150
43	8.06	973	1120	1290	1450	1610	729	847	970	1090	1210
44	8.44	1010	1180	1350	1520	1690	764	887	1010	1140	1260
45	8.83	1060	1230	1410	1590	1770	799	927	1060	1190	1320
46	9.22	1110	1290	1480	1670	1840	835	969	1110	1250	1380
47	9.62	1160	1340	1540	1740	1930	871	1010	1160	1300	1440
48	10.04	1210	1400	1610	1810	2010	909	1050	1200	1360	1510
49	10.46	1260	1460	1680	1890	2010	947	1100	1260	1420	1570
50	11.34	1370	1590	1820	2060	2000	1030	1190	1370	1540	1710
51	11.88	1430	1660	1900	2000	2370	1030	1240	1420	1600	1780
52	12.32	1430	1720	1900	2140	2370	1110	1240	1420	1670	1850
53	12.75	1540	1790	2050	2310	2560	1150	1340	1540	1730	1920
54	13.30	1600	1860	2130	2400	2660	1200	1390	1600	1800	1990
55	13.73	1660	1930	2210	2490	2760	1240	1440	1660	1870	2070
56	14.28	1720	2000	2290	2580	2860	1290	1500	1720	1940	2140
57	14.82	1780	2070	2370	2680	2960	1340	1550	1780	2010	2220
58	15.37	1850	2140	2460	2770	3070	1380	1610	1840	2080	2300
59	15.91	1910	2220	2540	2870	3180	1430	1660	1910	2150	2380
60	16.46	1980	2290	2630	2970	3280	1480	1720	1970	2220	2460
61	17.00	2040	2370	2720	3070	3390	1530	1780	2040	2300	2540
62	17.55	2110	2450	2810	3170	3510	1580	1840	2110	2370	2630
63	18.09	2180	2530	2900	3270	3620	1630	1900	2170	2450	2710
64	18.64	2250	2610	2990	3370	3740	1680	1960	2240	2530	2800
65	19.29	2320	2690	3090	3480	3860	1740	2020	2310	2610	2890
66	19.84	2390	2780	3180	3590	3980	1790	2080	2390	2690	2980
67	20.49	2460	2860	3280	3700	4100	1850	2150	2460	2770	3070
68	21.04	2540	2950	3380	3810	4220	1900	2210	2530	2860	3160
69	21.69	2610	3040	3480	3920	4350	1960	2280	2610	2940	3260
70	22.35	2690	3120	3580	4040	4470	2020	2340	2680	3030	3350

The nominal length mass values are for fully plasticated ropes. Subject to a tolerance of minus 2% to plus 5%. Balance ropes are normally designed to achieve a desired weight. Ropes with the required weight and strength will be designed to meet particular shaft requirements. Diameter: Off tension diameter subject to a tolerance of minus 0% to plus 4.5%.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product. Read cautionary notice - Restrictions on the use of large diameter multi-strand ropes.



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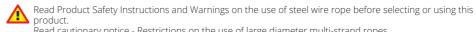
# Tiger 34M

## Hoist & Balance Rope

Lay Type		Lay Direction		Fin	ish	Core		
Ord	Ord Langs		Left Hand	Bright Galv		NFC	SFC	WSC
•	•	•	•	•	•	•	•	•

Diameter	Approx		Calculated	Aggregate Bre	eaking Force		Calculated Minimum Breaking Force				
Diameter	Mass	Balance 1180 N/mm ²	Balance 1370 N/mm ²	Balance & Hoist 1570 N/mm ²	Hoist 1770 N/mm ²	Hoist 1960 N/mm²	Balance 1180 N/mm ²	Balance 1370 N/mm ²	Balance & Hoist 1570 N/mm ²	Hoist 1770 N/mm²	Hoist 1960 N/mm ²
mm	kg/m	kN	kN	kN	kN	kN	kN	kN	kN	kN	kN
16	1.02	134	156	179	202	223	101	117	134	151	167
17	1.15	152	176	202	228	252	114	132	151	171	189
18	1.29	170	197	226	255	283	127	148	170	191	212
19	1.44	189	220	252	284	315	142	165	189	213	236
20	1.60	210	244	280	315	349	157	183	210	236	262
21	1.76	232	269	308	348	385	174	202	231	261	289
22	1.93	254	295	338	382	423	191	221	254	286	317
23	2.11	278	323	370	417	462	208	242	277	313	346
24	2.30	303	351	403	454	503	200	263	302	341	377
25	2.50	328	381	437	493	546	246	286	328	370	409
26	2.70	355	413	473	533	590	240	309	354	400	409
20		383			575	637		334	382		
	2.91		445	510			287			431	477
28	3.13	412	479	548	618	685	309	359	411	464	513
29	3.36	442	513	588	663	735	331	385	441	497	551
30	3.60	473	549	630	710	786	355	412	472	532	590
31	3.84	505	587	672	758	840	379	440	504	568	630
32	4.09	538	625	716	808	895	404	469	537	606	671
33	4.35	573	665	762	859	951	429	499	571	644	713
34	4.62	608	706	809	912	1010	456	529	607	684	757
35	4.90	644	748	857	967	1070	483	561	643	725	803
36	5.18	682	791	907	1020	1130	511	593	680	767	849
37	5.47	720	836	958	1080	1190	540	627	718	810	897
38	5.77	759	882	1010	1130	1260	569	661	758	854	946
39	6.08	800	929	1060	1200	1320	600	696	798	900	997
40	6.40	842	977	1120	1260	1390	631	733	840	947	1040
41	6.72	884	1020	1170	1320	1460	663	770	882	995	1100
42	7.05	928	1070	1230	1390	1540	696	808	926	1040	1150
43	7.39	973	1120	1290	1450	1610	729	847	970	1090	1210
44	7.74	1010	1180	1350	1520	1690	764	887	1010	1140	1260
45	8.1	1060	1230	1410	1590	1770	799	927	1060	1190	1320
46	8.5	1110	1290	1480	1670	1840	835	969	1110	1250	1380
47	8.8	1160	1340	1540	1740	1930	871	1010	1160	1300	1440
48	9.2	1210	1400	1610	1810	2010	909	1050	1200	1360	1510
49	9.6	1260	1460	1680	1890	2090	947	1100	1260	1420	1570
50	10.40	1370	1590	1820	2060	2280	1030	1190	1370	1540	1710
51	10.90	1430	1660	1900	2000	2370	1030	1240	1420	1600	1780
52	11.30	1430	1720	1900	2230	2470	1110	1240	1420	1670	1850
53			1720	2050	2230	2560		1340		1730	1920
54	11.70	1540					1150		1540		
	12.20	1600	1860	2130	2400	2660	1200	1390	1600	1800	1990
55	12.60	1660	1930	2210	2490	2760	1240	1440	1660	1870	2070
56	13.10	1720	2000	2290	2580	2860	1290	1500	1720	1940	2140
57	13.60	1780	2070	2370	2680	2960	1340	1550	1780	2010	2220
58	14.10	1850	2140	2460	2770	3070	1380	1610	1840	2080	2300
59	14.60	1910	2220	2540	2870	3180	1430	1660	1910	2150	2380
60	15.10	1980	2290	2630	2970	3280	1480	1720	1970	2220	2460
61	15.60	2040	2370	2720	3070	3390	1530	1780	2040	2300	2540
62	16.10	2110	2450	2810	3170	3510	1580	1840	2110	2370	2630
63	16.60	2180	2530	2900	3270	3620	1630	1900	2170	2450	2710
64	17.10	2250	2610	2990	3370	3740	1680	1960	2240	2530	2800
65	17.70	2320	2690	3090	3480	3860	1740	2020	2310	2610	2890
66	18.20	2390	2780	3180	3590	3980	1790	2080	2390	2690	2980
67	18.80	2460	2860	3280	3700	4100	1850	2150	2460	2770	3070
68	19.30	2540	2950	3380	3810	4220	1900	2210	2530	2860	3160
69	19.90	2610	3040	3480	3920	4350	1960	2280	2610	2940	3260
70	20.50	2690	3120	3580	4040	4470	2020	2340	2680	3030	3350

The nominal length mass values are for fully lubricated ropes. Balance ropes are normally designed to achieve a desired weight. Ropes with the required weight and strength will be designed to meet particular shaft requirements.



Read cautionary notice - Restrictions on the use of large diameter multi-strand ropes.









# Tiger Dyform 18M/PI

Balance Rope

Lay Type • • • • • • • .

D	A	Calculate	ed Aggregate Breaki	ng Force	Calculated Minimum Breaking Force			
Diameter	Approx Mass	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²	
mm	kg/m	kN	kN	kN	kN	kN	kN	
16	1.25	222	251	278	178	201	222	
17	1.42	251	283	314	201	226	251	
18	1.59	282	318	352	225	254	281	
19	1.77	314	354	392	251	283	313	
20	1.96	348	392	434	278	314	347	
21	2.17	384	432	479	307	346	383	
22	2.38	421	475	526	337	380	420	
23	2.60	460	519	575	368	415	460	
24	2.83	501	565	626	401	452	500	
25	3.07	544	613	679	435	490	543	
26	3.32	588	663	734	470	530	587	
27	3.58	634	715	792	507	572	634	
28	3.85	682	769	852	546	615	681	
29	4.13	732	825	914	585	660	731	
30	4.42	783	883	978	626	706	782	
31	4.72	836	943	1040	669	754	835	
32	5.03	891	1000	1110	713	804	890	
33	5.35	948	1060	1180	758	855	947	
34	5.68	1000	1130	1250	805	907	1000	
35	6.02	1060	1200	1330	853	962	1060	
36	6.37	1120	1270	1400	902	1010	1120	
37	6.73	1190	1340	1480	953	1070	1190	
38	7.10	1250	1410	1560	1000	1130	1250	
39	7.48	1320	1490	1650	1050	1190	1320	
40	7.90	1380	1560	1730	1110	1250	1380	
41	8.30	1450	1640	1820	1160	1310	1450	
42	8.72	1530	1720	1910	1220	1380	1520	
43	9.14	1600	1800	2000	1280	1440	1600	
44	9.57	1670	1890	2090	1340	1510	1670	
45	10.00	1750	1980	2190	1400	1580	1750	
46	10.40	1830	2060	2290	1460	1650	1830	
47	10.90	1910	2160	2390	1530	1720	1910	
48	11.30	1990	2250	2490	1590	1800	1990	
49	11.80	2080	2340	2600	1660	1870	2080	
50	12.30	2160	2440	2700	1730	1950	2160	
51	12.80	2250	2540	2810	1800	2030	2250	
52	13.30	2340	2640	2920	1870	2110	2340	
53	13.80	2430	2740	3040	1940	2190	2430	
54	14.40	2530	2850	3150	2020	2280	2520	

The nominal length mass values are for fully lubricated ropes.



Read cautionary notice - Restrictions on the use of large diameter multi-strand ropes.



This table is for guidance purposes only with no guarantee or warranty (express or implied) as to its accuracy. The products described may be subject to change without notice, and should not be relied on without further advice from Bridon-Bekaert.

# Tiger Superflex 17x6, 20x6 Balance Rope

	Lay Type		Lay Direc	tion		Finish	inish Core		
Ord	Lang	s Rig	ght Hand	Left Hand	Bright	Gal	lv N	FC SFC	IWRC
	•		•	•	•	•		• •	
Available as st	andard.								
Nominal	Nominal	Ca	Calculated Aggregate Breaking Force				Iculated Minim	um Breaking Fo	rce
Diameter	Length Mass	1080 N/mm²	1270 N/mm²	1370 N/mm²	1570 N/mm²	1080 N/mm²	1270 N/mm²	1370 N/mm²	1570 N/mm²
mm	kg/m	kN	kN	kN	kN	kN	kN	kN	kN
17x6									
44	7.31	856	1007	1086	1244	706	830	896	1026
46	7.63	917	1078	1163	1333	757	890	960	1100
47	7.96	930	1094	1180	1352	767	902	973	1115
48	8.29	962	1131	1220	1398	794	934	1007	1154
49	8.92	1020	1199	1294	1483	842	990	1068	1224
51	9.33	1083	1274	1374	1574	894	1051	1134	1300
54	10.83	1239	1457	1572	1801	1022	1202	1296	1486
57	11.95	1356	1595	1720	1971	1119	1316	1419	1627

20x6									
48	8.58	981	1154	1244	1426	809	951	1026	1176
51	9.75	1150	1325	1459	1672	949	1116	1204	1380
54	11.12	1308	1538	1659	1901	1079	1269	1369	1569
57	12.05	1408	1656	1786	2047	1162	1366	1474	1689
60	13.04	1524	1792	1933	2215	1257	1478	1595	1827
64	15.10	1767	2078	2241	2569	1458	1715	1850	2120
67	16.79	1963	2308	2490	2854	1620	1905	2055	2355
70	17.33	2028	2385	2573	2948	1674	1969	2124	2434
73	19.59	2247	2642	2850	3266	1854	2180	2352	2695

The nominal length mass values are for fully lubricated ropes. Balance ropes are normally designed to achieve a desired weight. Ropes with the required weight and strength will be designed to meet particular shaft requirements.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this Read Pro product.

Read cautionary notice - Restrictions on the use of large diameter multi-strand ropes.







# 8x4x7, 6x4x12, 8x4x14, 8x4x19

Flat Blance Rope

	Construction		Finish			
Single Stitched	Double Stitched	Bright Galv				
•	•	•	•	•		
Available as standard						

Nominal D Width x b x		Nominal Diameter of the	Sum of the Nominal Cross- Sectional Areas		ed Mass Per Unit he Lubricated Ro		Load at a Ter	egate Breaking nsile Grade of Vires
Double Stitched (d)	Single Stitched (e) or Clamped (k)	Load Carrying Wires	of the Load Carrying Wires	Double Stitched (d)	Single Stitched (e)	Clamped (k)	1370 N/mm²	1570 N/mm²
mm	mm	mm	mm²	kg/m	kg/m	kg/m	kN	kN
Rone Constru	uction 8 x 4 x 7	7 = 8 Legs with 4	1 Strands each	having 1+6 Wir	es = 224 wires			
110 x 20	110 x 18	1.9	635	6.42	6.16	6.04	870	997
113 x 20	113 x 18	1.95	669	6.76	6.49	6.36	917	1050
116 x 21	116 x 19	2.0	704	7.11	6.83	6.69	964	1105
119 x 21	119 x 19	2.05	739	7.47	7.17	7.02	1010	1160
122 x 22	122 x 20	2.1	776	7.84	7.53	7.38	1060	1220
125 x 22	125 x 20	2.15	813	8.22	7.89	7.73	1110	1280
128 x 23	128 x 21	2.2	851	8.60	8.26	8.09	1170	1340
Rope Constr	uction 6 x 4 x 1	2 = 6 Legs with	4 Strands each	h having 3+9 W	ires = 288 wires			
112 x 26	112 x 23	1.9	817	8.26	7.93	7.68	1120	1280
115 x 25	115 x 23	1.95	860	8.69	8.35	8.09	1180	1350
118 x 27	118 x 24	2.0	905	9.14	8.78	8.51	1240	1420
121 x 27	121 x 24	2.05	951	9.61	9.23	8.94	1300	1490
124 x 28	124 x 25	2.1	998	10.10	9.68	9.39	1370	1570
127 x 28	127 x 25	2.15	1046	10.60	10.20	9.84	1430	1640
130 x 29	130 x 26	2.2	1095	11.10	10.70	10.30	1500	1720
Rope Constru 146 x 25	uction 8 x 4 x 1 146 x 23	2 K= 8 Legs wit 1.9	h 4 Strands ea 1089	ch having 3+9 v 11.00	Vires = 384 wire 10.60	es 10.30	1490	1710
140 x 25 149 x 26	140 x 23	1.95	1147	11.60	11.20	10.80	1570	1800
154 x 27	154 x 24	2.0	1206	12.20	11.70	11.40	1650	1890
157 x 27	157 x 24	2.05	1267	12.20	12.30	11.90	1740	1990
160 x 28	160 x 25	2.05	1330	13.50	12.90	12.50	1820	2090
165 x 28	165 x 25	2.15	1394	14.10	13.60	13.10	1910	2190
168 x 29	168 x 26	2.2	1460	14.80	14.20	13.80	2000	2290
		4 K= 8 Legs wit	h 4 Strand <u>s ea</u>	ch having 4+10	Wires = 448 wir			
168 x 28	168 x 25	2.0	1407	14.30	13.70	13.30	1930	2210
172 x 29	172 x 26	2.05	1479	15.00	14.40	13.90	2030	2320
176 x 29	176 x 26	2.1	1552	15.70	15.10	14.60	2130	2440
180 x 30	180 x 27	2.15	1626	16.50	15.80	15.30	2230	2550
184 x 30	184 x 27	2.2	1703	17.20	16.60	16.00	2330	2670
				0	12 Wires = 608			
186 x 31	186 x 28	1.9	1724	17.50	16.80	16.20	2360	2710
190 x 32	190 x 29	1.95	1816	18.40	17.80	17.00	2490	2850
194 x 33	194 x 30	2.0	1910	19.30	18.60	18.00	2620	3000
200 x 34 204 x 34	200 x 31 204 x 31	2.05 2.1	2007 2106	20.30 21.30	19.50 20.40	18.90 19.80	2750 2890	3150 3310
204 x 34 210 x 36	204 x 31 210 x 32	2.1	2106	21.30	20.40	20.80	2890	3310 3460
210 x 36 216 x 37	210 x 32 216 x 33	2.15	2207	23.30	21.40	20.80	3020	3460
210 x 57	210 x 55	2.2	2311	25.50	22.40	21.00	5170	0000

The nominal length mass values are for fully lubricated ropes.





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# Tiger Full Lock Winding Rope

Lay Type		Lay Direction		Fin	ish	Core			
Ord	Langs	Right Hand	Left Hand	Bright	Galv	NFC	SFC	WSC	
		•	•	•	•				
Available as standard. Variable Torque and Turn characteristics available by design									

Nominal		Calculated Aggreg	ate Breaking Force	Calculated Minimu	m Breaking Force
Diameter	Nominal Length Mass	Standard Grade	Higher Grade	Standard Grade	Higher Grade
mm	kg/m	kN	kN	kN	kN
16	1.44	261	281	218	234
17	1.63	261	281	218	234
18	1.83	331	355	276	297
19	2.04	368	395	307	330
21	2.49	449	483	375	403
21.5	2.60	465	500	388	417
22	2.73	493	530	412	443
24	3.25	587	631	490	527
26	3.81	689	740	575	618
27	4.11	743	798	620	667
29	4.74	856	921	715	769
30	5.08	916	985	765	822
31	5.42	928	998	775	833
32	5.78	1043	1121	871	936
33	6.14	1109	1192	926	995
35	6.91	1246	1339	1040	1118
37	7.72	1398	1502	1167	1255
37.5	7.93	1422	1528	1187	1276
38	8.14	1468	1578	1226	1318
40	9.02	1634	1756	1364	1466
40.5	9.25	1668	1793	1393	1497
41	9.48	1715	1844	1432	1539
42	9.95	1798	1932	1501	1614
43	10.40	1880	2021	1570	1688
44	10.90	1974	2122	1648	1772
45	11.40	2068	2223	1727	1857
46	11.90	2162	2324	1805	1940
47	12.50	2244	2413	1874	2015
48	13.00	2350	2526	1962	2109
49	13.50	2443	2626	2040	2193
51	14.70	2655	2854	2217	2383
52	15.00	2738	2943	2286	2457
53	15.80	2867	3082	2394	2574
54	16.40	2972	3195	2482	2668
55	17.00	3055	3284	2551	2742
56	17.70	3195	3435	2668	2868
57	18.30	3313	3561	2766	2973
59	19.60	3501	3763	2923	3142
60	20.30	3630	3902	3031	3258
62	21.70	3865	4155	3227	3469
64	23.10	4123	4433	3443	3701
65	23.80	4253	4572	3551	3817

The nominal length mass values are for fully lubricated ropes.

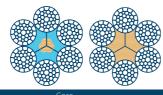








# Tiger Dyform 6R 6x36 (WS) Hoist Rope

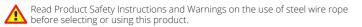


Lay	iype	Lay Di	rection	FIN	lisn	Core			
Ord	Langs	Right Hand	Left Hand	Bright	Galv	NFC	SFC	IWRC	BRISTAR
•	•	•	•	•	•	•	•	•	•
Available as standa	ard. IWRC values avai	lable on request							

Diamatas		Calcula	ted Aggregate Breaki	ng Force	Calculate	ed Minimum Break	ing Force
Diameter	Approx Mass	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²
mm	kg/m	kN	kN	kN	kN	kN	kN
25	2.64	450	507	562	391	441	489
26	2.86	487	549	608	423	477	529
27	3.08	525	592	655	457	515	570
28	3.32	564	636	705	491	554	613
29	3.56	606	683	756	527	594	658
30	3.81	648	731	809	564	636	704
31	4.07	692	780	864	602	679	752
32	4.33	737	831	921	641	723	801
33	4.61	784	884	979	682	769	852
34	4.89	833	939	1030	724	817	904
35	5.19	882	995	1100	768	865	958
36	5.49	933	1050	1160	812	916	1010
37	5.80	986	1110	1230	858	967	1070
38	6.11	1040	1170	1290	905	1020	1130
39	6.44	1090	1230	1360	953	1070	1190
40	6.77	1150	1290	1430	1000	1130	1250
41	7.12	1210	1360	1510	1050	1180	1310
42	7.47	1270	1430	1580	1100	1240	1380
43	7.83	1330	1500	1660	1150	1300	1440
44	8.20	1390	1570	1740	1210	1360	1510
45	8.6	1450	1640	1820	1260	1430	1580
46	9.0	1520	1710	1900	1320	1490	1650
47	9.4	1590	1790	1980	1380	1560	1720
48	9.8	1660	1870	2070	1440	1620	1800
49	10.1	1730	1950	2160	1500	1690	1870
50	10.5	1800	2030	2240	1560	1760	1950
51	11.0	1870	2110	2330	1630	1830	2030
52	11.4	1940	2190	2430	1690	1910	2110
53	11.9	2020	2280	2520	1760	1980	2190
54	12.3	2100	2360	2620	1820	2060	2280
55	12.8	2170	2450	2720	1890	2130	2360
56	13.2	2250	2540	2820	1960	2210	2450
57	13.7	2340	2630	2920	2030	2290	2540
58	14.2	2420	2730	3020	2100	2370	2630
59	14.7	2500	2820	3130	2180	2460	2720
60	15.2	2590	2920	3230	2250	2540	2810
61	15.7	2680	3020	3340	2330	2630	2910
62	16.2	2770	3120	3450	2400	2710	3000
63	16.8	2860	3220	3570	2480	2800	3100
64	17.3	2950	3320	3680	2560	2890	3200
65	17.9	3040	3430	3800	2640	2980	3300
66	18.4	3130	3530	3910	2730	3070	3400

The nominal length mass values are for fully lubricated ropes.

Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.





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Tiger Hoist Ro		5x36	(WS)						
Lay 1	уре	Lay Dir	rection	Fin	ish		C	ore	
Ord				Bright	Galv	NFC	SFC	IWRC	BRISTAR
•	• • • •				•	•	•	•	•
Available as standa	ard. IWRC values avail								

Diamatas		Calcula	ted Aggregate Breaki	ng Force	Calculate	ed Minimum Breaki	ng Force
Diameter	Approx Mass	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²
mm	kg/m	kN	kN	kN	kN	kN	kN
22	1.86	317	357	396	276	311	344
23	2.04	347	391	433	301	340	376
24	2.22	377	425	471	328	370	410
25	2.41	409	462	511	356	402	445
26	2.60	443	499	553	385	434	481
27	2.81	478	539	597	416	469	519
28	3.02	514	579	642	447	504	558
29	3.24	551	621	688	479	541	599
30	3.47	590	665	737	513	579	641
31	3.70	630	710	787	548	618	684
32	3.94	671	757	838	584	658	729
33	4.19	714	805	891	621	700	775
34	4.45	758	854	946	659	743	823
35	4.72	803	905	1000	699	788	872
36	4.99	850	958	1060	739	833	923
37	5.27	898	1010	1120	781	880	975
38	5.56	947	1060	1180	824	929	1020
39	5.86	997	1120	1240	868	978	1080
40	6.17	1040	1180	1310	913	1020	1130
41	6.48	1100	1240	1370	959	1080	1190
42	6.80	1150	1300	1440	1000	1130	1250
43	7.13	1210	1360	1510	1050	1180	1310
44	7.46	1270	1430	1580	1100	1240	1370
45	7.8	1320	1490	1650	1150	1300	1440
46	8.2	1380	1560	1730	1200	1360	1500
47	8.5	1440	1630	1800	1260	1420	1570
48	8.9	1510	1700	1880	1310	1480	1640
49	9.3	1570	1770	1960	1370	1540	1710
50	9.6	1630	1840	2040	1420	1600	1780
51	10.0	1700	1920	2130	1480	1670	1850
52	10.4	1770	1990	2210	1540	1730	1920
53	10.8	1840	2070	2300	1600	1800	2000
54	11.2	1910	2150	2380	1660	1870	2000
55	11.6	1980	2230	2470	1720	1940	2150
56	12.0	2050	2310	2560	1780	2010	2230
57	12.5	2130	2400	2660	1850	2090	2310
58	12.9	2200	2480	2750	1910	2160	2390
59	13.4	2280	2570	2850	1980	2230	2480
60	13.8	2360	2660	2940	2050	2310	2560
61	14.3	2440	2750	3040	2120	2390	2650
62	14.8	2520	2840	3140	2120	2470	2730
63	15.3	2600	2930	3250	2260	2550	2820
64	15.6	2680	3020	3350	2330	2630	2910
65	16.2	2770	3120	3460	2330	2710	3010
66	16.7	2850	3220	3560	2480	2800	3100
00	10.7	2000	5220	5500	2,00	2000	5100

The nominal length mass values are for fully lubricated ropes. Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.

Read pages Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.



# Tiger Dyform 6R 6x19 (S)



Lay 1	Туре	Lay Di	rection	Fin	ish		Core	
Ord	Langs	Right Hand	Left Hand	Bright	Galv	NFC	SFC	IWRC
•	•	•	•	•	•	•	•	•
Available as standar	d IMPC values available	o op roquoct						

Diameter	Approx Mass	Calculate	d Aggregate Breaking	Force	Calculate	ed Minimum Breaki	ng Force
Diameter	Approximass	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²
mm	kg/m	kN	kN	kN	kN	kN	kN
25	2.64	451	508	563	392	442	490
26	2.86	488	550	609	424	478	530
27	3.08	526	593	657	457	516	571
28	3.32	566	638	706	492	555	614
29	3.56	607	684	758	528	595	659
30	3.81	649	732	811	565	637	705
31	4.07	693	782	866	603	680	753
32	4.33	739	833	923	643	725	803
33	4.61	786	886	981	684	771	854
34	4.89	834	941	1040	726	818	906
35	5.19	884	997	1100	769	867	960
36	5.49	935	1050	1160	814	917	1010
37	5.80	988	1110	1230	860	969	1070
38	6.11	1040	1170	1300	907	1020	1130
39	6.44	1090	1230	1370	955	1070	1190
40	6.77	1150	1300	1440	1000	1130	1250
41	7.12	1210	1360	1510	1050	1190	1310
42	7.47	1270	1430	1590	1100	1240	1380

The nominal length mass values are for fully lubricated ropes.

Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.

Read Product Safety Instructions and Warnings on the use of steel wire rope Read Product Safety Instructions and a before selecting or using this product.



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# Tiger 6R 6x19 (S)

Lay Type		Lay Direction		Finish		Core				
Ord	Ord Langs Right Hand Left Hand		Bright Galv		NFC SFC IWRC					
•	•	•	•	•	•	•	•	•		
Available as standar	Available as standard. IWRC values available on request									

Diameter		Calculate	d Aggregate Breaking	Force	Calculate	ed Minimum Breaki	ng Force
Diameter	Approx Mass	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²
mm	kg/m	kN	kN	kN	kN	kN	kN
16	0.95	163	183	203	141	160	177
17	1.08	184	207	229	160	180	200
18	1.21	206	232	257	179	202	224
19	1.35	230	259	287	200	225	249
20	1.49	254	287	318	221	250	276
21	1.64	281	316	350	244	275	305
22	1.81	308	347	385	268	302	335
23	1.97	337	380	420	293	330	366
24	2.15	367	413	458	319	360	398
25	2.33	398	449	497	346	390	432
26	2.52	430	485	537	374	422	467
27	2.72	464	523	580	404	455	504
28	2.93	499	563	623	434	490	542
29	3.14	536	604	669	466	525	582
30	3.36	573	646	716	499	562	623
31	3.59	612	690	764	532	600	665
32	3.82	652	735	814	567	640	708
33	4.07	694	782	866	603	680	753
34	4.32	736	830	919	641	722	800
35	4.58	780	880	974	679	765	848
36	4.84	826	931	1030	718	810	897
37	5.12	872	983	1080	759	855	947
38	5.40	920	1030	1140	800	902	999
39	5.68	969	1090	1210	843	950	1050
40	5.98	1010	1140	1270	887	1000	1100
41	6.28	1070	1200	1330	932	1050	1160
42	6.59	1120	1260	1400	978	1100	1220

The nominal length mass values are for fully lubricated ropes. Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.







# Tiger 6R 6x7



**@** 

• • • • • • • • • Available as standard. IWRC values available on request

Diameter	Approx Mass	Calculated Aggreg	ate Breaking Force	Calculated Minimu	um Breaking Force
Diameter	Approx Mass	1570 N/mm ²	1770 N/mm ²	1570 N/mm ²	1770 N/mm ²
mm	kg/m	kN	kN	kN	kN
13	0.59	103	116	90.1	101
14	0.69	120	135	104	117
15	0.79	137	155	120	135
16	0.90	156	176	136	153
17	1.01	177	199	154	173
18	1.14	198	223	172	194
19	1.27	221	249	192	217
20	1.41	245	276	213	240
21	1.55	270	304	235	265
22	1.70	296	334	258	291
23	1.86	324	365	282	318
24	2.03	353	398	307	346
25	2.20	383	431	333	375
26	2.38	414	467	360	406
27	2.57	446	503	388	438
28	2.76	480	541	418	471
29	2.96	515	581	448	505
30	3.17	551	622	480	541
31	3.38	589	664	512	577
32	3.61	627	707	546	615
33	3.83	667	752	580	654
34	4.07	708	798	616	695
35	4.31	750	846	653	736

The nominal length mass values are for fully lubricated ropes. Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.



Tiger 6T Bristar Compound & 6T Compound Layer 6x26, 6x27, Hoist Rope											
Lay 1	Гуре	Lay Di	rection	Fin	ish		Core				
Ord	Langs	Right Hand	Left Hand	Bright	Galv	NFC	SFC	BRISTAR			
	· · · · · · · · ·										

	Approx	Cal	culated Aggreg	ate Breaking Fo	orce	Ca	lculated Minim	um Breaking Fo	orce
Diameter	Mass	1570 N/mm ²	1770 N/mm²	1960 N/mm ²	2160 N/mm ²	1570 N/mm ²	1770 N/mm ²	1960 N/mm²	2160 N/mm ²
mm	kg/m	kN	kN	kN	kN	kN	kN	kN	kN
28	3.40	563	625	685		484	538	589	
29	3.61	597	664	727		514	571	625	
30	3.93	649	721	790		558	620	679	
31	4.13	683	758	830		587	652	713	
32	4.45	738	820	897		634	705	772	
33	4.67	771	857	938		663	737	807	
34	4.98	824	916	1003		709	787	862	
35	5.30	877	974	1066		754	838	917	
36	5.64	933	1036	1135		802	891	976	
37	5.88	971	1078	1181		835	927	1015	
38	6.23	1030	1144	1253		886	984	1077	
39	6.61	1096	1218	1333		943	1047	1146	
40	6.98	1157	1285	1407		995	1105	1210	
41	7.28	1204	1338	1465		1035	1150	1259	
42	7.57	1253	1392	1524		1077	1197	1310	
43	8.05	1333	1482	1622		1147	1274	1395	
44	8.38	1387	1541	1687	1841	1192	1325	1451	1583
45	8.79	1456	1618	1772	1933	1252	1391	1524	1663
46	9.13	1512	1680	1839	2006	1300	1444	1581	1725
47	9.46	1569	1742	1907	2081	1349	1498	1640	1789
48	10.00	1659	1843	2017	2201	1427	1585	1735	1893
49	10.45	1735	1927	2110	2303	1492	1658	1815	1980
50	10.85	1800	2000	2189	2388	1548	1720	1882	2054
51	11.26	1866	2073	2269	2476	1605	1783	1951	2129
52	11.88	1969	2187	2395	2613	1693	1881	2059	2247
53	12.23	2028	2253	2468	2694	1744	1938	2122	2317
54	12.67	2098	2331	2553	2786	1804	2005	2195	2396
55	12.95	2146	2384	2610	2848	1845	2050	2244	2449
56	13.41	2218	2464	2697	2943	1907	2119	2319	2531
57	14.05	2330	2588	2834	3093	2003	2226	2437	2660
58	14.53	2405	2672	2925		2068	2298	2516	
59	14.97	2481	2756	3018		2134	2370	2595	
60	15.46	2559	2842	3111		2200	2444	2676	
61	15.92	2638	2929	3207		2268	2519	2758	
62	16.66	2759	3065	3356		2373	2636	2886	
63	16.91	2799	3108	3402		2407	2673	2926	
64	17.68	2924	3248	3555		2515	2793	3058	
65	18.41	3056	3394	3716		2628	2919	3195	

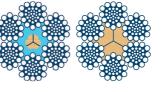
The nominal length mass values are for fully lubricated ropes. Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.



Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.



# Tiger 6T Bristar Compound & 6T Compound Layer 6x22, 6x23, 6x25



# Hoist and Haulage Rope

Lay	Туре	Lay Di	Lay Direction		Finish			Core		
Ord	Ord Langs		Left Hand	Bright Galv		NFC	SFC	BRISTAR		
	•	•	•	•	•	•	•	•		

	A M	Calculate	ed Aggregate Break	ing Force	Calculat	ed Minimum Breaki	ng Force
Diameter	Approx Mass	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²	1570 N/mm ²	1770 N/mm ²	1960 N/mm ²
mm	kg/m	kN	kN	kN	kN	kN	kN
16	1.10	183	204	223	157	175	192
17	1.23	205	229	251	177	197	216
18	1.40	232	259	284	200	222	244
19	1.55	258	287	315	222	247	271
20	1.73	288	321	352	247	276	303
21	1.91	319	355	389	274	305	335
22	2.08	346	385	423	298	331	364
23	2.30	383	427	468	329	367	403
24	2.50	416	464	509	358	399	437
25	2.71	451	502	551	387	432	474
26	2.88	479	534	586	412	459	504
27	3.10	516	575	631	444	494	543
28	3.36	561	625	686	482	537	590
29	3.62	605	674	739	520	579	635
30	3.91	653	728	798	562	626	687
31	4.17	696	776	851	599	667	732
32	4.38	732	815	894	629	701	769
33	4.65	777	866	950	668	744	817
34	5.03	841	937	1028	723	806	884
35	5.25	876	976	1071	753	839	921
36	5.61	935	1042	1143	804	896	983
37	5.85	975	1086	1192	838	934	1025
38	6.19	1032	1150	1261	888	989	1085
39	6.57	1099	1225	1344	945	1053	1155
40	6.85	1143	1273	1396	982	1094	1201
41	7.26	1213	1351	1483	1043	1162	1275
42	7.54	1258	1402	1538	1082	1206	1323
43	7.97	1332	1484	1629	1146	1277	1401
44	8.26	1380	1537	1687	1187	1322	1451
45	8.71	1457	1624	1782	1253	1396	1533
46	9.05	1513	1685	1849	1301	1449	1590
47	9.55	1596	1778	1950	1373	1529	1677
48	9.91	1657	1846	2026	1425	1587	1742
49	10.25	1712	1907	2093	1472	1640	1799
50	10.77	1800	2005	2200	1548	1725	1892

The nominal length mass values are for fully lubricated ropes. Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.



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U	6T Si ) Hoist ar	U	_ayer ge Rope	6x8, (	5x10			>
Lay 1	Гуре	Lay Di	rection	Fin	ish	Co	re	
Ord	Langs	Right Hand	Left Hand	Bright	Galv	NFC	SFC	
•	•	•	•	•	•	•	•	

Diameter	Approx Mass	Calculated Aggre	gate Breaking Force	Calculated Minimu	Calculated Minimum Breaking Force		
Diameter	Approximass	1570 N/mm²	1770 N/mm ²	1570 N/mm ²	1770 N/mm ²		
mm	kg/m	kN	kN	kN	kN		
13	0.69	110	124	96	108		
14	0.80	127	144	111	126		
15	0.92	146	165	128	144		
16	1.05	166	187	145	164		
17	1.19	188	212	164	185		
18	1.33	210	237	184	208		
19	1.48	234	264	205	231		
20	1.64	260	293	227	256		
21	1.81	286	323	251	283		
22	1.98	314	354	275	310		
23	2.17	344	387	301	339		
24	2.36	374	422	327	369		
25	2.56	406	458	355	400		
26	2.77	439	495	384	433		
27	2.99	474	534	414	467		
28	3.22	509	574	446	502		
29	3.45	546	616	478	539		
30	3.69	585	659	512	577		
31	3.94	624	704	546	616		
32	4.20	665	750	582	656		
33	4.47	707	797	619	698		
34	4.74	751	847	657	741		
35	5.02	796	897	696	785		

The nominal length mass values are for fully lubricated ropes.

Ropes for friction winding application will weigh approximately 2% less than the above quoted weights.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.



# Tiger Half Lock

# Guide/Rubbing Rope

Lay	Туре	Lay Di	rection	Fin	ish		Core	
Ord	Langs	Right Hand	Left Hand	Bright	Galv	NFC	SFC	WSC
		•	•	•	•			

Nominal	Nominal Longth Mass	Calculated Aggreg	ate Breaking Force	Calculated Minimum Breaking Force		
Diameter	Nominal Length Mass	Standard Grade	Higher Grade	Standard Grade	Higher Grade	
mm	kg/m	kN	kN	kN	kN	
29	4.63	455	546	421	505	
32	5.63	554	665	512	614	
35	6.74	663	796	613	736	
38	7.94	781	937	722	866	
41	9.25	909	1091	841	1009	
45	11.10	1092	1310	1010	1212	
48	12.70	1241	1489	1148	1378	
51	14.30	1411	1693	1305	1566	
52	14.95	1704	1942	1576	1796	
54	16.34	1845	2110	1707	1952	

The nominal length mass values are for fully lubricated ropes.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this 



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# 

Lay Туре		Lay Dir	rection	Fin	ish	Core
Ord	Langs	Right Hand	Left Hand	Bright	Galv	Modified Core
	•	•		•	•	•

Nominal		Calculated Minimum Breaking Load					
Diameter	Nominal Length Mass	Grade 1670 N/mm ²	Grade 1670 N/mm ²	Grade 1820 N/mm ²	Grade 1820 N/mm ²		
mm	kg/m	tonnes	kN	tonnes	kN		
6x19S							
32	3.94	59.51	584	64.40	632		
33	4.19	63.28	621	68.48	672		
34	4.45	67.18	659	72.70	713		
35	4.71	71.19	698	77.04	756		
36	4.99	75.31	739	81.50	800		
37	5.27	79.56	780	86.09	845		
38	5.56	83.91	823	90.81	891		
39	5.85	88.39	867	95.65	938		
40	6.16	92.98	912	100.62	987		
41	6.47	97.69	958	105.71	1037		
6x26WS							
41	6.51	98.25	964	106.33	1043		
42	6.83	103.10	1011	111.58	1095		
43	7.16	108.07	1060	116.95	1147		
44	7.49	113.16	1110	122.46	1201		
45	7.84	118.36	1161	128.09	1257		
46	8.53	127.20	1248	137.65	1350		
47	8.91	132.79	1303	143.70	1410		
48	9.29	138.50	1359	149.88	1470		
49	9.68	144.33	1416	156.19	1532		
50	10.08	150.28	1474	162.63	1595		
51	10.49	156.35	1534	169.20	1660		
52	10.90	162.54	1595	175.90	1726		
6x31WS							
41	6.69	100.97	991	109.28	1072		
42	7.02	105.95	1039	114.68	1125		
43	7.36	111.06	1089	120.21	1179		
44	7.70	116.28	1141	125.86	1235		
45	8.06	121.63	1193	131.65	1291		
46	8.77	130.71	1282	141.48	1388		
47	9.15	136.45	1339	147.70	1449		
48	9.55	142.32	1396	154.05	1511		
49	9.95	148.32	1455	160.54	1575		
50	10.36	154.43	1515	167.15	1640		
51	10.78	160.67	1576	173.91	1706		
52	11.21	167.03	1639	180.79	1774		
53	11.64	173.52	1702	187.82	1843		
54	12.08	180.13	1767	194.97	1913		
55	12.54	186.86	1833	202.26	1984		
56	13.00	193.72	1900	209.68	2057		
57	13.46	200.80	1969	217.23	2131		
58	13.94	207.80	2039	224.92	2206		
59	14.43	215.03	2109	232.75	2283		
60	13.88	222.38	2182	240.70	2361		

#### The nominal length mass values are for fully lubricated ropes.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.





# Tiger Dyform Bristar CDR



Lay ٦	Гуре	Lay Di	rection	Fin	ish	Core
Ord	Langs	Right Hand	Left Hand	Bright	Galv	BRISTAR
	•	•			•	•

Nominal	Dopo Waight	Calculated Aggreg	ate Breaking Load	Calculated Minim	um Breaking Load
Diameter	Rope Weight	1670	1820	1670	1820
mm	kg/m	kN	kN	kN	kN
6x19S					
32	4.05	785	855	683	744
33	4.31	835	910	726	791
34	4.58	886	966	771	840
35	4.84	939	1020	817	890
36	5.13	993	1080	864	942
37	5.42	1040	1140	913	995
38	5.71	1100	1200	963	1040
39	6.02	1160	1270	1010	1100
40	6.33	1220	1330	1060	1160
41	6.65	1280	1400	1120	1220
6x25WS					
42	6.98	1350	1470	1170	1280
43	7.32	1410	1540	1230	1340
44	7.66	1480	1610	1290	1400
45	8.02	1550	1690	1350	1470
46	8.38	1620	1760	1410	1530
47	8.74	1690	1840	1470	1600
48	9.11	1760	1920	1530	1670
49	9.51	1840	2000	1600	1740
50	9.90	1910	2080	1660	1810
51	10.29	1990	2170	1730	1890
52	10.68	2070	2250	1800	1960
6x31WS	44.07	2450	22.40	4070	20.40
53	11.07	2150	2340	1870	2040
54	11.47	2230	2430	1940	2120
55	11.96	2310	2520	2010	2190
56	12.35	2400	2620	2090	2280
57	12.84	2490	2710	2160	2360
58	13.23	2570	2810	2240	2440
59	13.72	2660	2900	2320	2530
60	14.21	2760	3000	2400	2610

The nominal length mass values are for fully lubricated ropes.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.



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# Tiger Dyform 6CDR

Lay 1	Гуре	Lay Direction			
Ord	Langs	Right Hand	Left Hand		
	•	•			
Available as standa	rd. Bristar values availa	ble on request			

Nominal	Nominal Length Mass	Calculated Minimu	Im Breaking Force
Diameter	Norminal Length Mass	Grade 1670 N/mm ²	Grade 1820 N/mm ²
mm	kg/m	kN	kN
6x19S			
32	4.33	683	744
33	4.6	726	791
34	4.89	771	840
35	5.19	817	890
36	5.49	864	942
37	5.79	913	995
38	6.11	963	1040
39	6.44	1010	1100
40	6.77	1060	1160
41	7.11	1120	1220
42	7.46	1170	1280
43	7.82	1230	1340
6x31WS			
44	8.18	1290	1400
45	8.55	1350	1470
46	8.92	1410	1530
47	9.30	1470	1600
48	9.70	1530	1670
49	10.10	1600	1740
50	10.50	1660	1810
51	10.90	1730	1890
52	11.30	1800	1960
53	11.70	1870	2040
54	12.20	1940	2120
55	12.60	2010	2190
56	13.10	2090	2280
57	13.50	2160	2360
58	14.00	2240	2440
59	14.50	2320	2530
60	14.99	2400	2610

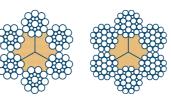
The nominal length mass values are for fully lubricated ropes.



Fin	ish		Core	
Bright	Galv	NFC	SFC	Bristar
•	•	•	•	



# Tiger 6CDR 6x19(S), 6x25(F)



Lay Type		Lay Di	rection	Finish		Core		
Ord	Langs	Right Hand	Left Hand	Bright	Galv	NFC	SFC	Bristar
	•	•		•	•	•	•	
Available as standar	rd. Bristar values availa	ble on request						

Nominal	Nominal Length Mass	Calculated Minimu	num Breaking Force	
Diameter	Nominal Length Mass	Grade 1670 N/mm ²	Grade 1820 N/mm ²	
mm	kg/m	kN	kN	
32	3.82	604	658	
33	4.07	642	700	
34	4.32	681	743	
35	4.58	722	787	
36	4.84	764	833	
37	5.12	807	880	
38	5.40	851	928	
39	5.68	897	977	
40	5.98	943	1020	
41	6.15	1010	1100	
42	6.45	1060	1160	
43	6.76	1110	1210	
44	7.08	1170	1270	
45	7.40	1220	1330	
46	7.74	1270	1390	
47	8.08	1330	1450	
48	8.43	1390	1510	
49	8.78	1450	1580	
50	9.14	1510	1640	
51	9.51	1570	1710	
52	9.89	1630	1780	
53	10.20	1690	1850	
54	10.60	1760	1920	
55	11.00	1820	1990	
56	11.40	1890	2060	
57	11.80	1960	2140	
58	12.30	2030	2210	
59	12.70	2100	2290	
60	13.10	2170	2370	

#### The nominal length mass values are for fully lubricated ropes.

Read Product Safety Instructions and Warnings on the use of steel wire rope before selecting or using this product.



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# technical information.



# 1. Hoist Ropes

Various constructions of ropes may be used for hoisting, the final choice usually being decided upon economic grounds. What may be a satisfactory life on a shallow high frequency hoist, may be completely uneconomic on a deep low frequency installation, and therefore the rope designs as well as their sizes must be considered.

1.1 Drum Hoists

6 Stranded Ropes – both round and triangular strand – are satisfactory for all depths of shafts, although perhaps best suited for those up to 1000m in depth with fixed guides. They are not suitable for shafts deeper than 600m with rope guides, as their natural tendency to twist causes the conveyance

to turn.

As a rough guide to the construction of the rope, the ratio of drum or sheave diameter to outer wire diameter should be between 1000 and 1500:1, although if abrasion is severe this can be reduced slightly at the expense of a lower fatigue life.

For maximum resistance to wear and crossover damage the use of Lang's lay is recommended.

Multi-Strand Rotation Resistant Ropes – are now used on permanent drum hoist installations, except where multi-layer coiling is employed, due to their relatively low resistance to compressive forces. Certain constructions are suitable for sinking purposes.

Multi-strand ropes with Dyformed (compacted) strands have increased resistance to crushing over ropes with conventional strands.

Locked Coil Ropes – have gained in popularity and are extensively used throughout the UK. They can be used to advantage on any depth of shaft with either fixed or rope guides. As they are virtually non-rotating under normal loading conditions they are considered to be the best rope to operate in shafts deeper than 700 metres equipped with rope guides.

The cross section is extremely compact and as a result such ropes can withstand very high radial and compressive forces This property coupled with their smooth outer surface enables them to be used to advantage on multilayer coiling installations. Because of their compact cross section, it is desirable that the drum or sheave diameter to rope diameter ratio should be in the region of 100 to 120:1 for satisfactory service life on main shaft winders and for kibble ropes used in shaft sinking. Ratios as low as 50:1 can be tolerated on small ropes in shallow shafts, staple shafts and sinking stage winders.

1.2 Friction or Koepe Hoists

6 Stranded Ropes – are suitable to depths of 1000 metres. Beyond that the torque in these ropes can result in premature torsional fatigue of the wires. Triangular strands are more suited due to the lower contact pressures on the friction linings although Lang's lay equal laid round strand ropes are quite suitable for shallow shafts. Round strand ropes with Dyformed (compacted) strands are becoming more popular as they offer higher breaking loads, increased fatigue life and reduced contact pressures over ropes with conventional strands.

With rope guided shafts, alternate left and right hand lay ropes are employed to prevent conveyance twist.

Tread pressures with stranded ropes are limited to 17.5 kgf/cm2 (1.72Mpa) to avoid excessive wear of the friction linings.

Multi-Strand Rotation Resistant Ropes – can be usefully employed at all depths of shaft and generally satisfactory lives are obtained. Earlier designs of the ropes were subject to severe internal cross-cutting. However modern designs incorporating Dyformed (compacted) strands and plastic enhancement coupled with modern manufacturing techniques.

Tread pressure limits are similar to those of 6 stranded ropes.

Locked Coil Ropes – are widely used on this type of hoist particularly in the UK. The advantages offered by ropes of this construction make them particularly suited for this type of hoist especially if rope guides are employed.

Due to the large smooth surface area of locked coil ropes, tread pressures of up to 28.0 kgf/cm2 (2.75MPa) can be tolerated. The limit is used to minimise friction liner wear, the rope being able to withstand much higher pressures.

1.3 Recommended Rope Constructions for various winder applications

applications	
Type of winder application	Rope Construction
Small drum hoist operating at less than 2.5m/s in a vertical shaft with fixed guides	6x19(9/9/1) FC Langs Lay Full Locked Coil
Small Drum hoist operating in a vertical shaft with rope guides	Multi-strand Rotation Resistant Full Locked Coil
Large drum hoist operating in a vertical shaft with fixed guides	Compound Triangular Strand Langs Lay Full Locked Coil Dyform 6R Ordinary/Langs Lay
Large drum hoist operating in a vertical shaft with rope guides	Multi-strand Rotation Resistant Full Locked Coil
Blair multi-rope hoist	Compound Triangular Strand Langs Lay Full Locked Coil
Friction hoist operating to a depth of 500m	6 strand Ordinary/Langs Lay Compound Triangular Strand Langs Lay Multi-strand Rotation Resistant Full Locked Coil Dyform 6R Ordinary/Langs Lay
Friction hoist operating to a depth between 500m and 1000m	6 Strand Ordinary/Langs Lay Compound Triangular Strand Langs Lay Multi-strand Rotation Resistant Full Locked Coil Dyform 6R Ordinary/Langs Lay
Friction Hoists above 1000m	Locked Coil Winding Ropes Mult-strand Rotation Resistant Dyform 6R Ordinary/Langs Lay Compound Triangular Strand Langs Lay
Sinking stage winder	Multi-strand Rotation Resistant Full Locked Coil Alternate Lay Triangular Strand Langs Lay
Kibble winder	Multi-strand Rotation Resistant Full Locked Coil
	Multi-strand Rotation Resistant Superflex Flat rope

# 2. Sinking Ropes

Kibble Ropes – Ropes used for these duties must be rotation resistant, to prevent excessive spin of the kibble or bucket in the shaft.

Providing the hoist equipment is suitable, flexible full locked coil ropes meet these requirements admirably, and have been used successfully for many years. Where very small diameter sinking drums and sheaves are employed, or where a sheave is fitted above the kibble to enable two parts of rope to support the load, multi-strand rotation resistant ropes are recommended.

Bridon's dedicated Mining Department will be pleased to discuss and recommend the best rope construction for optimum performance on your kibble winder.

Stage Ropes – There are several methods of suspending the sinking stage or platform and this can govern the choice of rope construction.

Stage ropes are normally required to act has guide ropes for the kibble, so resistance to wear is a necessary characteristic. In addition, a good resistance to crushing on multi-layer drum coiling is required.

Full locked coil ropes offer excellent performance on the correct design of equipment.

Where smaller drums and sheaves are employed multistrand rotation resistant ropes with relatively large outer wires or triangular strands with equal numbers of left and right hand lay can be used. With triangular strand ropes however, problems can be experienced with controlling the turn if slack rope conditions occur.

Bridon's dedicated Mining Department will be pleased to discuss and recommend the best rope construction for optimum performance on your stage winder.

Under normal circumstances it is recommended that ropes for both applications, but in particular stage ropes, should be manufactured from galvanised material. However, where higher tensile grades of wire are required galvanised material is not always available. In these cases it is strongly recommended that the ropes are regularly cleaned and re-lubricated with emphasis on the evaluation of corrosion during examination.

# 3. Balance Ropes

Generally balance ropes are required to have the flexibility to suit the particular cage centres, adequate rotation resistant properties combined with good resistance to wear and corrosion. Bridon's range of multi-strand rotation resistant and Flat Balance ropes have the capability to meet the needs for all balance rope applications.

Bridon-Bekaert's Superflex balance ropes were developed for installations where maximum flexibility is required combined with optimum resistance to wear and corrosion. The range of ropes is almost completely non-rotating, however it is common industry practice to also use a swivel within the attachment assembley. As a result there is no torsional effect either at the terminal ends or at the loop and therefore the onset of fatigue at these points is almost entirely eliminated. However it is common industry practice to also incorporate a balance rope swivel within the rope attachment assembly

Where maximum flexibility is not required alternative constructions are available to suit the specific winding conditions and provide optimum service life.

The graph below gives the minimum recommended loop diameter to rope diameter ratio for various constructions.



For advice on the best rope for your installations contact Bridon's dedicated Mining Department.

# 4. Guide and Rubbing Ropes

Bridon-Bekaert's Tiger Brand range of guide and rubbing ropes are normally constructed of a central king wire, covered by one or two layers of round wires which are closed in a final layer of half lock and round wires. The precise construction depends upon the diameter and the tensile grade of wires used to meet the breaking force requirement. Bridon's CAD rope design system ensures that the largest possible outer half lock and round wires are used to give maximum resistance to wear and corrosion. The choice of size and breaking load depends upon the local regulations for factor of safety and the tensioning required. A typical arrangement is a factor of safety of 5:1 at the point of suspension with the guides tensioned on the basis of 3000kg plus 500kg for each 100m of shaft depth. The tensions are normally varied in the range plus or minus 10% to limit harmonic vibration.

In wet and corrosive shafts the use of galvanised material is recommended.

Types of tensioning arrangement, terminations and methods of installation are many and varied, Bridon's dedicated Mining Department will be pleased to give advice on these aspects along with types of layouts, methods of lubrication, inspection procedures and maintenance.

# 5. Haulage Ropes

The modern rope haulage system is an integral part of the system for both the transportation of men and the supply of materials to the mine face.

Haulage systems fall into 3 main categories Endless Direct Main and Tail

Bridon Bekaert's Tiger Brand range has the rope to suit your system.

In general, haulage ropes are required to have excellent resistance to wear and in some instances corrosion. To achieve this they tend to be of the more simple construction with fewer larger outer wires. These can be single layer round strand construction or triangular strand construction. On the majority of systems where the length of travel is high and the frequency of cycle is small, fatigue is generally not a critical deteriorating factor.

5.1 Single Construction

#### Round Strand

6x7(6/1) Fibre Core Langs lay is recommended to maximise the resistance to wear.

Triangular Strand 6x8TS, 6x9TS, 6x10TS.

However, when travel distances become shorter and the cycle frequency is higher then fatigue can become a factor dictating rope removal, particularly when drive wheels, drums and sheaves are smaller. To combat this, more complex (compound constructions) with smaller outer wires can be used.

5.2 Compound Construction

Round Strand 6x7, 6x19(S), Dyform 6x19(S), 6x22(TS).

Triangular Strand 6x22TS, 6x23TS, 6x25TS, 6x28TS.

Where wet and corrosive conditions exist the use of

On certain installations where resistance to crushing is required, then the use of ropes with steel IWRC cores should be considered.

On endless systems, ropes with special preforming are supplied to facilitate long splicing.

The performance of round strand ropes can be enhanced by the use of Dyformed strands. Dyform ropes offer the following improvements:-

- Higher breaking loads
- Improved fatigue life
- Increased resistance to crushingReduced interference on drums and Clifton
- (surge) wheels

Bristar Cores offer the following improvements:-

- Reduced stretch
- Increased fatigue life
- Increased dimension stability (diameter retention)

Contact our dedicated Mining Department for advice on the best construction for your haulage application.

# 6. Conveyor Drive Ropes

Bridon-Bekaert has had a close working relationship with the OEM's of cable driven conveyors for many years. This has resulted in Bridon being the major supplier of cable belt driving ropes world wide. Extensive research and development has resulted in Bridon's Tiger Brand range of driving ropes such that Bridon can offer rope solutions to give optimum lowest cost conveying of material.

The Tiger Brand range offers the following rope options:-

Conventional Driving Ropes 6x19S, 6x26WS, 6x25F, 6x31WS, 6x36WS.

The type of construction used depends upon the diameter, stress levels, the type of conveyor and it's layout.

Dyform Driving Ropes 6x19S Dyform, 6x26WS Dyform, 6x31WS Dyform, 6x36WS Dyform.

Dyform Driving Ropes offer the following advantages:-

- Higher breaking forces
- Increased fatigue life
- Increased resistance to wear
- Reduced line stand pulley wear during the early part of service life

Driving ropes are generally supplied in galvanised material although ropes manufactured from bright wire are available. They are produced under the highest quality system from high specification wire and cores specially designed and manufactured for use on rope driven conveyors. All ropes have specific strand preformation to facilitate long splicing and maximise splice life. In both conventional and Dyform drive ropes, alternative cores and manufacturing lubrication are available to best suit your conveyor conditions to ensure maximum economic operating performance. These include the following:-

- Man made fibre cores for use in wet conditions
- Bristar cores offering lower stretch, increased fatigue life and improve diameter retention
- Special lubrication, both manufacturing and service, to ensure maximum life in severe corrosive conditions

#### Zebra Drive Ropes

Joint development with rope driven conveyor manufacturers and operators has resulted in Bridon's Zebra range of conveyor drive ropes.

Extensive laboratory and on site testing has shown the following advantages of Zebra over conventional and Dyform drive ropes:

- Increased fatigue life. In excess of 10 times conventional cables in laboratory tests
- Equivalent or increased breaking loads
- Reduced stretch both constructional and elastic
- Superior diameter retention
- Smooth outer surface
- Reduced tread pressures
- Superior resistance to internal corrosion

These improvements in physical properties have realised the following proven cost saving advantages:

- · Zebra can be retro fitted to existing
- conveyors at minimal cost
- Reduced line pulley wear
- Reduced steel terminal pulley and surge/Koepe
- lining maintenance
- Reduced vibration and noise
- Extended rope life
- Extended splice life

For an assessment of potential cost saving on your conveyor contact Bridon directly.

Bridon's commitment to lowest cost conveying doesn't stop there. On long conveyors splicing and splice maintenance can be both inconvenient and costly. Bridon's unique Service Department can provide expert engineers to install, splice, inspect and maintain your drive cables. Driving ropes are a major cost component part of the conveyor. LOOK AFTER THEM !

In addition Bridon-Bekaert recognised the implications of down time and cost of splicing on long conveyors with numerous splices. To minimise splicing and splice repairs Bridon increased its production capacity from piece weights of 60 tonnes to piece weights of approximately 135 tonnes. If you think longer ropes can assist in reducing operating costs contact our Mining Department who will be pleased to discuss the

various options.

# 7. Properties of Extension of Steel Wire Ropes

Any assembly of steel wires spun into a helical formation, either as a strand or wire rope, when subjected to a tensile load, can extend in three separate phases, depending on the magnitude of the applied load.

There are also other factors which produce rope extension which are very small and can normally be ignored.

Phase 1 - Initial or Permanent Constructional Extension

At the commencement of loading a new rope, extension is created by the bedding down of the assembled wires with a corresponding reduction in overall diameter. This reduction in diameter creates an excess length of wire which is accommodated by a lengthening of the helical lay. When sufficiently large bearing areas have been generated on adjacent wires to withstand the circumferential compressive loads, this mechanically created extension ceases and the extension in Phase 2 commences. The Initial Extension of any rope cannot be accurately determined by calculation and has no elastic properties.

The practical value of this characteristic depends upon many factors, the most important being the type and construction of rope, the range of loads and the number and frequency of the cycles of operation. It is not possible to quote exact values for the various constructions of rope in use, but the following approximate values may be employed to give reasonably accurate results.

The above figures are for guidance purposes. More precise figures are available upon request.

#### Locked Coil Hoist Ropes

	% of rope	e length
	Fibre Core	Steel Core
Lightly loaded Factor of safety about 8:1	0.25	0.125
Normally loaded Factor of safety about 5:1	0.50	0.25
Heavily loaded Factor of safety about 3:1	0.75	0.50
Heavily loaded with many bends and/or deflections	Up to 2.00	Up to 1.00

Immediate permanent extension	0.08
Additional initial extension	0.08
Gradual permanent extension	0.08
Total extension approx.	0.25

#### Phase 2 - Elastic Extension

Following Phase 1, the rope extends in a manner which complies approximately with Hookes Law (stress is proportional to strain) until the Limit of Proportionality or Elastic Limit is reached.

It is important to note that wire ropes do not possess a Young's Modulus of Elasticity, however an 'apparent' Modulus of Elasticity can be

#### determined between two fixed loads.

The Modulus of Elasticity also varies with different rope constructions, but generally increases as the cross-sectional area of steel increases. By using the values given, it is possible to make a reasonable estimate of elastic extension, but if greater accuracy is required it is advisable to carry out a modulus test on an actual sample of the rope. As rope users will find it difficult to calculate the actual metallic steel area , the values normally quoted are based on the circumscribed rope area (area of a circle, related to the nominal diameter of the rope).

#### Elastic Extension = $\frac{WL}{EA}$ (mm)

W = load applied (kgs)

- L = rope length (mm)
- E = elastic modulus (kg/mm²)
- A = circumscribed rope area (mm²)

#### Phase 3 - Permanent Extension

The permanent, non-elastic extension of the steel caused by tensile loads exceeding the yield point of the material.

If the load exceeds the Limit of Proportionality, the rate of extension will accelerate as the load is increased, until a loading is reached at which continuous extension will commence, causing the wire rope to fracture without any further increase of load.

Thermal Expansion and Contraction

The coefficient of linear expansion ( $_{\Pi}$ ) of steel wire rope is 0.0000125 = (12.5 x10⁻⁶) per °C, therefore the change in length of 1 metre of rope produced by a temperature change of t °C would be;

Change in length  $\Delta | = \prod |_{\circ} t$  where

- $\Pi$  = coefficient of linear expansion
- | eriginal length of rope (m)
- t = temperature change (°C)

The change will be an increase in length if the temperature rises and a decrease in length if the temperature falls.

Extension due to Rotation

The elongation caused by a free rope end being allowed to rotate.

Extension due to Wear

The elongation due to inter-wire wear which reduces the cross-sectional area of steel and produces extra constructional extension.

Example: What will be the total elongation of a 200 metre length of 28mm diameter Tiger 6R wire rope at a tension of 10 tonnesf (tf) and an increase in temperature of  $20^{\circ c}$ .

Permanent Constructional Extension = 0.25% of rope length = 500mm

Elastic Extension =  $\frac{WL}{EA} = \frac{10000 \times 200\ 000}{6000 \times 615.8} = 540$ mm

Thermal Expansion =  $\Delta 1 = \Box \mid : t = 0.0000125 \times 200,000 \times 20 = 50mm$ Therefore total extension = 500 + 540 + 50 = 1090mm

# 8. Pressures between Ropes and Sheaves or Drums

In addition to the bending stresses experienced by wire ropes operating over sheaves or pulleys, ropes are also subjected to radial pressure as they make contact with the sheave. This pressure sets up shearing stresses in the wires, distorts the rope's structure and affects the rate of wear of the sheave grooves. When a rope passes over a sheave, the load on the sheave results from the tension in the rope and the angle of rope contact. It is independent of the diameter of the sheave.

Load on bearing =  $2T \sin \theta$ 

T = rope tension (kg)

 $\theta$  = contact angle between rope and sheave or drum

Assuming that the rope is supported in a well fitting groove, then the pressure between the rope and the groove is dependent upon the rope tension and diameter but is independent of the arc of contact.

Pressure, P =  $\frac{2T}{R}$ 

- $P = \text{pressure} (\text{kg/cm}^2)$
- T = rope tension (kg)
- D = diameter of sheave or drum (cm)
- d = diameter of rope (cm)

#### Maximum Permissible Pressures

	Groove material				
Number of outer wires in strands	Cast iron	Low carbon cast steel	11 to 13% Mn steel or equivalent alloy steels kgf/cm ²		
	kgf/cm ²	kgf/cm ²			
5 - 8 Ordinary lay	20	40	105		
5 - 8 Lang's lay	25	45	120		
9 - 13 Ordinary lay	35	60	175		
9 - 13 Lang's lay	40	70	200		
14 - 18 Ordinary lay	42	75	210		
14 - 18 Lang's lay	47	85	240		
Triangular strand	55	100	280		

It should be emphasised that this method of estimation of pressure assumes that the area of contact of the rope in the groove is on the full rope diameter, whereas in fact only the crowns of the outer wires are actually in contact with the groove. The local pressures at these contact points may be as high as 5 times those calculated and therefore the values given above cannot be related to the compressive strength of the groove material.

If the pressure is high, the compressive strength of the material

in the groove may be insufficient to prevent excessive wear and indentation and this in turn will damage the outer wires of the rope and effect its working life. As with bending stresses, stresses due to radial pressure increase as the diameter of the sheave decreases. Although high bending stresses generally call for the use of flexible rope constructions having relatively small diameter outer wires, these have less ability to withstand heavy pressures than do the larger wires in the less flexible constructions. If the calculated pressures are too high for the particular material chosen for the sheaves or drums or indentations are being experienced, consideration should be given to an increase in sheave or drum diameter. Such a modification would not only reduce the groove pressure, but would also improve the fatigue life of the rope.

The pressure of the rope against the sheave also causes distortion and flattening of the rope structure. This can be controlled by using sheaves with the correct groove profile which, for general purposes, suggests an optimum groove radius of nominal rope radius +10%. The profile at the bottom of the groove should be circular over an angle of approximately 120°, and the angle of flare between the sides of the sheave should be

Rope grade			oximate dness
Min. Tensile Strength	API 9A Grade	Brinel	Rockwell 'C'
2160N / mm ²	EEIPS	480 / 500	52
1960N / mm ²	EIPS	470 / 480	51
1770N / mm ²	IPS	445 / 470	49
1570N / mm ²	PS	405 / 425	45

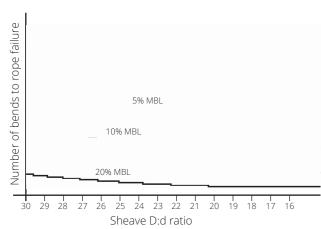
Suggested pulley hardness: 250-300 Brinell for Mn steel or equivalent alloy steel.

# 9. Bend Fatigue

Bend fatigue testing of ropes usually consists of cycling a length of rope over a sheave while the rope is under a constant tension as part of its ongoing development programme Bridon has tested literally thousands of ropes in this manner over the years on its in-house own design bend testing equipment.

Through this work, Bridon has been able to compare the effects of rope construction, tensile strength, lay direction, sheave size, groove profile and tensile loading on bend fatigue performance under ideal operating conditions. At the same time it has been possible to compare rope life to discard criteria (e.g. as laid down in ISO 4309) with that to complete failure of the rope, i.e. to the point where the rope has been unable to sustain the load any longer. As part of the exercise, it has also been possible to establish the residual breaking strength of the rope at discard level of deterioration.

Effects of D:d Ratio and loading on fatigue life - Typical example Dyform 6



What

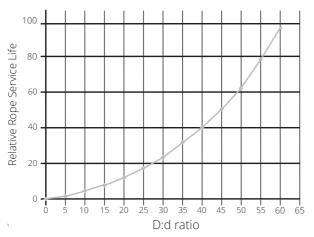
needs to be recognised, however, is that very few ropes operate under these controlled operating conditions, making it very difficult to use this base information when attempting to predict rope life under other conditions. Other influencing factors, such as dynamic loading, differential loads in the cycle, fleet angle, reeving arrangement, type of coiling on the drum, change in rope direction, sheave alignment, sheave size and groove profile, can have an equally dramatic effect on rope performance.

However, the benefit of such testing can be particularly helpful to the rope manufacturer when developing new or improving existing products.

If designers or operators of equipment are seeking optimum rope

performance or regard bending fatigue life as a key factor in the operation of equipment, such information can be provided by Bridon for guidance purposes.

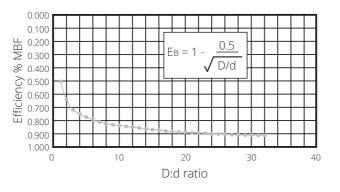
Service life curve for various D:d ratios



considering the use of a steel wire rope around a minimum D:d ratio, it is generally accepted that below 4:1, the effect on the strength of the rope needs to be considered. Permanent distortions within the rope will occur when using ratios of 10:1 or less, a minimum ratio of 16:1 should be used for a rope operating

#### around sheaves.

Approximate loss in breaking strength due to bending

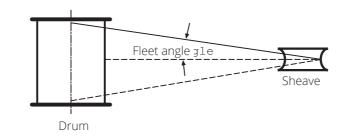


# 10. Fleet Angle

Of all the factors which have an influence on the winding of a rope on a smooth drum, the fleet angle, arguably, has the greatest effect.

Fleet angle is usually defined as the included angle between two lines, one which extends from a fixed sheave to the flange of a drum and the other which extends from the same fixed sheave to the drum in a line perpendicular to the axis of the drum. (See illustration).

Illustration of Fleet Angle



If the drum incorporates helical grooving, the helix angle of the groove needs to be added or subtracted from the fleet angle as described above to determine the actual fleet angle experienced by the rope.

#### At the drum

When spooling rope onto a drum it is generally recommended that the fleet angle is limited to between  $0.5^{\circ}$  and  $2.5^{\circ}$ . If the fleet angle is too small, i.e. less than  $0.5^{\circ}$ , the rope will tend to pile up at the drum flange and fail to return across the drum. In this situation, the problem may be alleviated by introducing a 'kicker' device or by increasing the fleet angle through the introduction of a sheave or spooling mechanism.

If the rope is allowed to pile up it will eventually roll away from the flange creating a shock load in both the rope and the structure of the mechanism, an undesirable and unsafe operating condition.

Excessively high fleet angles will return the rope across the drum prematurely, creating gaps between wraps of rope close to the flanges as well as increasing the pressure on the rope at the cross-over positions.

Even where helical grooving is provided, large fleet angles will inevitably result in localised areas of mechanical damage as the wires 'pluck' against each other. This is often referred to as 'interference' but the amount can be reduced by selecting a Langs lay rope if the reeving allows. The "interference" effect can also be reduced by employing a Dyform rope which offers a much smoother exterior surface than conventional rope constructions.

Floating sheaves or specially designed fleet angle compensating devices may also be employed to reduce the fleet angle effect.

#### At the sheave

Where a fleet angle exists as the rope enters a sheave, it initially makes contact with the sheave flange. As the rope continues to pass through the sheave it moves down the flange until it sits in the bottom of the groove. In doing so, even when under tension, the rope will actually roll as well as slide. As a result of the rolling action the rope is twisted, i.e. turn is induced

into or out of the rope, either shortening or lengthening the lay length of the outer layer of strands. As the fleet angle increases so does the amount of twist.

To reduce the amount of twist to an acceptable level the fleet angle should be limited to 2.5° for grooved drums and 1.5° for plain drums and when using rotation-resistant low rotation and parallel-closed ropes the fleet angle should be limited to 1.5°.

However, for some applications it is recognised that for practical reasons it is not always possible to comply with these general recommendations, in which case the rope life could be affected.

#### 11. Rope Torque

The problem of torsional instability in hoist ropes would not exist if the ropes could be perfectly torque balanced under load. The torque generated in a wire rope under load is usually directly related to the applied load by a constant 'torque factor'. For a given rope construction the torque factor can be expressed as a proportion of the rope diameter and this is shown below.

Variation with rope construction is relatively small and hence the scope for dramatically changing the stability of a hoisting system is limited. Nevertheless the choice of the correct rope can have a deciding influence, especially in systems which are operating close to the critical limit. It should be noted that the rope torque referred to here is purely that due to tensile loading. No account is taken of the possible residual torque due, for example, to rope manufacture or installation procedures.

Good installation practises are vital to prevent torque build up in your new rope. Winding system designers need to take this into consideration at the development stage. Bridon can advise on all mining installation process's.

#### Torsional Stability

The torque factors quoted on page 41 are approximate maximum values for the particular constructions. To calculate the torque value for a particular rope size multiply the rope diameter by the nominal rope diameter. Example: for 20mm dia. Tiger 34LR 34x7 Class at 20% of minimum breaking force:-

Torque value

- = torque factor x rope dia.
- = 0.8% x 20mm = 0.16mm
  - 16mm

# 11. Rope Torque

To calculate the torque generated in a particular rope when subjected to a tensile load, multiply the load by the torque value and combine the units.

Example: for 20mm dia. Tiger 34LR 34x7 Class at 6000 kg f load

Torque generated = torque value x load = 0.16 . 6000 = 960 kgf.mm

#### Bending Loads

As the rope is bent over the headsheave or drum, an additional force is induced into the steel which must be added to the static and dynamic tensions to obtain the total force imposed. There are many methods of calculation for this bending force, although the one most commonly used is:

Bending force = EdA D

where E = Elastic Modulus as given under

- 'Elongation of Wire Rope' kgf/mm² d = diameter of outer wire in rope – mm
- A = Cross sectional area of rope  $mm^2$
- D = Diameter of sheave or drum mm
- Size of Outer Wires in Rope

It is sometimes useful to know the size of the outer wires in ropes i.e. when estimating the amount of external wear or calculating bending stress. These can be calculated with reasonable accuracy for all constructions of 6 strand ropes using the following formula.

6 strand round strand

Diameter of outer wires = Nominal diameter of rope No. of outer wires per strand + 3

#### Example:

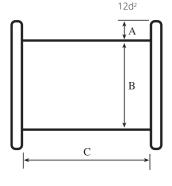
26mm diameter 6 x 36 (14/7 and 7/7/1) round strand No. of outer wires per strand = 14 Diameter of = 26 = 1.5mm outer wire 14+3

#### Calculations of Drum Capacity

The following formula gives an approximate indication regarding length of rope of a given diameter (d) which can be installed onto a winch/drum.

Imperial

Rope length (ft) = (A + B)  $\times$  A  $\times$  C  $\times$   $\pi$ 



#### Metric

Rope length (m) = (A + B) x A x C x  $\pi$  x 10⁶ d² where A, B and C are quoted in metres and d quoted in mm.

NOTE: Ropes are normally manufactured to a maximum oversize tolerance of 4%. Therefore the actual diameter 'd' could be nominal diameter + 4%.

#### **WARNING**

Wire rope will fail if worn-out, shock loaded, overloaded, misused, damaged, improperly maintained or abused.

•Always inspect wire rope for wear, damage or abuse before use

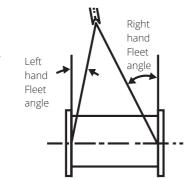
 Never use wire rope which is worn-out, damaged or abused

• Never overload or shock load a wire rope

 Inform yourself: Read and understand the guidance on product safety given in this catalogue; also read and understand the machinery manufacturer's handbook

 Refer to applicable directives, regulations, standards and codes concerning inspection, examination and rope removal criteria

Protect yourself and others - failure of wire rope may cause serious injury or death!





#### Rope Oscillation

Drum hoists operating with multiple layers of rope often experience severe oscillation of the rope between the headgear sheave and the hoist drum during some part of the hoisting cycle. Advice should be sought from BRIDON'S Mining Division.

# How to order hoist ropes

Cu	stomer information			
I.	Particulars of shaft:			
	Suspended Hoist Rope (From Lowest level to Headgear pulley)			
	Type of ventilation (upcast/downcast)			
	Shaft water inflow			
	pH value			
	Chloride content			
	Range of temperature variation Other conditions affecting the rope			
	Particulars of hoisting: Type of hoisting			
	Type of holding			
2.	Application			
-				
3.	Speed of lifting, m/sec			
4.	Acceleration of lifting, m/sec ²			
	Preventative deceleration, m/sec ²			
б.	Guides			
	Particulars of the winder:			
	Type Drum diameter			
	Drum diameter Drum width			
	Drum width Diameter of Headgear pulley, (mm)			
	Width of Headgear Pulley			
	Diameter tolerance taking into account the bottom of the pulley			
	Type of lining			
	Diameter of deflector sheave (Tower mounted Friction winding only)			
9.	Number of hoist ropes			
10.	Number of balance ropes			
	Type of balance ropes			
	Weight of 1 m of balance ropes			
	Loop radius of balance ropes			
	Particulars of the hoist conveyance:			
۱.	Mass of empty conveyance with suspension gear of hoist			
2	and balance ropes, tonnes Mass of conveyance (2) or counterweight with suspension gear, tonnes			
2. 3	Mass of payload, tonnes			
-	Number of cycles per day/month			
	Particulars of the rope:			
	Rope Specification			
2.	Nominal diameter, mm			
	Construction			
4.	Direction and type of lay			
5.	Type of core			
	Weight of 1 m, kg			
	Length of the rope, m			
	Number of individual lengths			
	Preferred Lubrication			
	Galvanised/Ungalvanised			
	Rope Tensile, kN/mm ²			
	Minimum Breaking Load, kgf Nominal Breaking Load, kgf			
	Aggr. Breaking Load of all wires, kgf			
	Lubrication			
	Minimum Safety Factor Required			
17.	Please state any local regulations that need to be adhered to			

ł								
	One Rope	Multirop	e N	lulti Lay	er Coiling	N	o. of Layers	5
	Cage	Skip	K	ibble	Cou	nterw	/eight	
	Mineral							
	Mineral & Ma	nriding						
	If Available							
	Rope		-					
	Rigid:	Wood	Stee	91	Rollers		Shoe	
	Drum Winde	er   Fricti	on Wind	er-towe	er or Groun	nd Mo	unted Dru	m
	Core:		rands:		Rope			
	Core: Aggregate E Minimum B	Breaking Lo	ad		Ropu Please tic			

# Summary Technical Information (For guidance purposes only)

Bridon supply a range of 'Tiger' High Performance steel wire ropes specifically designed and manufactured to meet the needs of today's mine winder specifications and the demanding applications to which they are exposed. High performance ropes are normally selected by customers when they require the specific characteristics of improved performance, high strength, low extension or low rotation.

Rope Construction	Rope Modulus at	Torque Factor at 20% of MBF			
hope construction	20% of MBF kN/mm ²	%			
		Ordinary	Langs		
TIGER 6R F 6 x 7 Class	61.80	8.1	12.0		
TIGER 6R F 6 x 19 Class	54.00	8.1	12.0		
TIGER 6R F 6 x 36 Class	50.80	8.1	12.0		
TIGER Dyform 6R F 6 x 7 Class	66.90	8.1	12.0		
TIGER Dyform 6R F 6 x 19 Class	54.20	8.1	12.0		
TIGER Dyform 6R F 6 x 36 Class	50.30	8.1	12.0		
TIGER 6T F 6 x 8 Class Single layer	68.70	n/a	13.4		
TIGER 6T F 6 x 25 Class Compound layer	61.80	n/a	13.4		
TIGER 18M F 18 x 7 Class	42.30	n/a	6.6		
TIGER 18M F 18 x 19 Class	41.80	n/a	6.6		
TIGER Dyform 18 18 x 7 Class	65.70	n/a	4.5		
TIGER Dyform 18 18 x 19 Class	65.70	n/a	4.5		
TIGER 34M F 34 x 7 Class	41.20	n/a	5.1		
TIGER 34M F 34 x 19 Class	40.70	n/a	5.1		
TIGER 34LR 34 x 7 Class	72.60	n/a	2.3		
TIGER 34LR 34 x 19 Class	72.60	n/a	2.3		
TIGER Superflex 14 x 6	40.20	n/a	3.9		
TIGER Superflex 17 x 6	38.30	n/a	2.6		
TIGER Superflex 20 x 6	36.30	n/a	1.3		
TIGER 6R CDR 6 x 19 Class	50.00	n/a	12.0		
TIGER 6R CDR 6 x 25 Class	46.40	n/a	12.0		
TIGER 6R CDR 6 x 31 Class	46.40	n/a	12.0		
TIGER Dyform 6R CDR 6 x 19 Class	54.20	n/a	12.0		
TIGER Dyform 6R CDR 6 x 26 Class	50.30	n/a	12.0		
TIGER Dyform 6R CDR 6 x 31 Class	50.30	n/a	12.0		
TIGER Zebra CDR 6 x 19	63.90	n/a	9.6		
TIGER Zebra CDR 6 x 26	59.30	n/a	9.6		
TIGER Zebra CDR 6 x 31	59.30	n/a	9.6		
TIGER FL Hoist Class	98.10		Variable		
TIGER FL Aerial Track Class	110.00		Variable		
TIGER HL Guide Class	117.00		Variable		
TIGER 24LS	67.2	n/a	5.8		
TIGER Dyform 24LS	77.6	n/a	5.8		
TIGER 34M SPI	40.7	n/a	5.1		

# Guide to Examination

The continued safe operation of lifting equipment, lifting accessories (e.g. slings) and other systems employing wire rope, depends on the operation of well programmed periodic rope examinations and the assessment by the competent person of the fitness of the rope for further service.

Examination and discard of ropes by the competent person should be in accordance with the instructions given in the original equipment manufacturer's handbook. In addition, account should be taken of any local or application specific Regulations.

The competent person should also be familiar, as appropriate, with the latest versions of related International, European or National standards such as ISO 4309

"Cranes - Wire ropes - code of practice for examination".

Particular attention must be paid to those sections of rope which experience has shown to be liable to deterioration. Excessive wear, broken wires, distortions and corrosion are the more common visible signs of deterioration.

Note: This publication has been prepared as an aid for rope examination and should not be regarded as a substitute for the competent person.

Wear is a normal feature of rope service and the use of the correct rope construction ensures that it remains a secondary aspect of deterioration. Lubrication may help to reduce wear.

Broken wires are a normal feature of rope service towards the end of the rope's life, resulting from bending fatigue and wear. The local break up of wires may indicate some mechanical fault in the equipment. Correct lubrication in service will increase fatigue performance.

Distortions are usually as a result of mechanical damage, and if severe, can considerably affect rope strength.

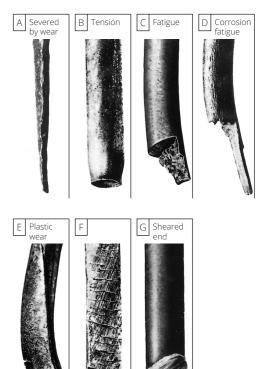
Visible rusting indicates a lack of suitable lubrication, resulting in corrosion. Pitting of external wire surfaces becomes evident in some circumstances. Broken wires ultimately result.

Internal corrosion occurs in some environments when lubrication is inadequate or of an unsuitable type. Reduction in rope diameter will frequently guide the observer to this condition. Confirmation can only be made by opening the rope with clamps or the correct use of spike and needle to facilitate internal inspection.

Note: Non-destructive testing (NDT) using electromagnetic means may also be used to detect broken wires and/or loss in metallic area. This method complements the visual examination but does not replace it.

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Some of the More Common Types of Wire Fractures Can Include:

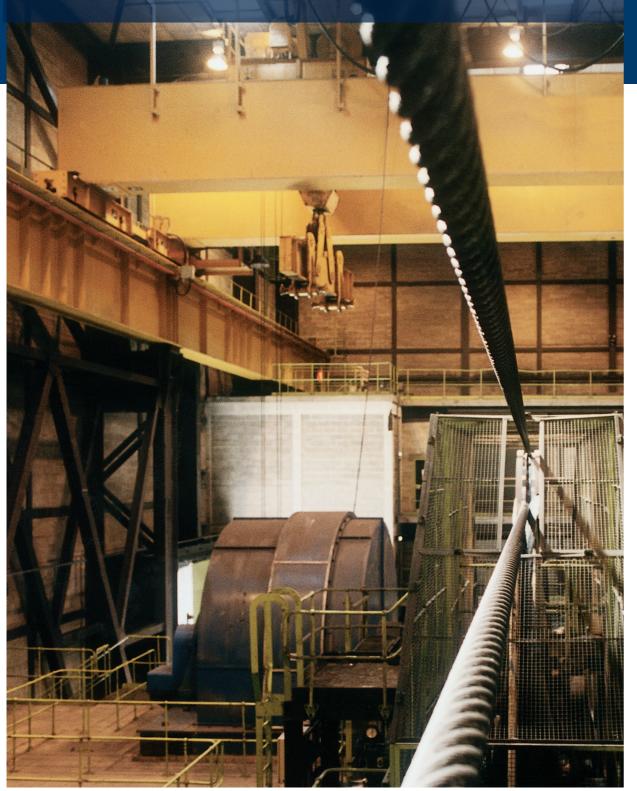


#### Factors Affecting Rope Performance

Multi-layer coiling of the rope on the drum can result in severe distortion in the underlying layers.

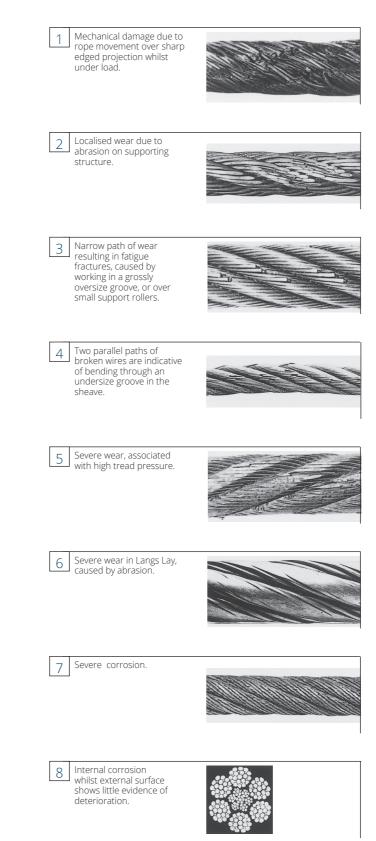
- Bad coiling (due to excessive fleet angles or slack winding) can result in mechanical damage, shown
- as severe crushing, and may cause shock loading during operation.
- Small diameter sheaves can result in permanent set of the rope, and will certainly lead to early wire breaks due to fatigue.
- Oversize grooves offer insufficient support to the rope leading to increased localised pressure, flattening of the rope and premature wire fractures. Grooves are deemed to be oversize when the groove diameter exceeds the nominal rope diameter by more than 15% steel, 20% polyurethane liners.
- Undersize grooves in sheaves will crush and deform the rope, often leading to two clear patterns of wear and associated wire breaks.
- Excessive angle of fleet can result in severe wear of the rope due to scrubbing against adjacent laps on the drum. Rope deterioration at the termination may occur in the form of broken wires. An excessive angle of fleet can also induce rotation causing torsional imbalance.

# troubleshooting guide.



# Troubleshooting Guide

Typical examples of Wire Rope deterioration



9	Typical wire fractures as a result of bend fatigue.	
10	Wire fractures at the strand, or core interface, as distinct from 'crown' fractures.	
11	Break up of IWRC resulting from high stress application.	
12	Looped wires as a result of torsional imbalance and/or shock loading.	
13	Typical example of localised wear and deformation.	
14	Multi-strand rope 'bird caged' due to torsional imbalance.	
15	Protrusion of rope centre resulting from build up of turn.	<u></u>
16	Substantial wear and severe internal corrosion.	

# Troubleshooting Guide

The following is a simplified guide to common wire rope problems. More detailed advice can be obtained from any Bridon distributor. In the event of no other standard being applicable, Bridon recommends that ropes are inspected/examined in accordance with ISO 4309.

Problem	Cause/Action
Mechanical damage caused by the rope contacting the	Generally results from operational conditions.
structure of the installation on which it is operating or an external structure - usually of a localised nature.	<ul> <li>Check sheave guards and support/guide sheaves to ensure that the rope has not "jumped out" of the intended reeving system.</li> </ul>
	Review operating conditions.
Opening of strands in rotation resistant, low rotation and parallel closed ropes - in extreme circumstances the rope may develop a "birdcage distortion" or protrusion of inner strands.	<ul> <li>Check sheave and drum groove radii using sheave gauge to ensure that they are no smaller than nominal rope radius +5% - Bridon recommends that the sheave and drum groove radii are checked prior to any rope installation.</li> </ul>
Note - rotation resistant and low rotation ropes are designed with a specific strand gap which may be apparent on delivery in an off tension	Repair or replace drum/sheaves if necessary.
condition. These gaps will close under load and will have no effect on the operational performance of the rope.	<ul> <li>Check fleet angles in the reeving system - a fleet angle in excess of 1.5 degrees may cause distortion.</li> </ul>
	<ul> <li>Check installation method - turn induced during installation can cause excessive rope rotation resulting in distortion.</li> </ul>
	<ul> <li>Check if the rope has been cut "on site " prior to installation or cut to remove a damaged portion from the end of the rope. If so, was the correct cutting procedure used? Incorrect cutting of rotation resistant, low rotation and parallel closed ropes can cause distortion in operation.</li> </ul>
	Rope may have experienced a shock load.
Broken wires or crushed or flattened rope on lower layers at crossover points in multi-layer coiling situations. Wire breaks usually resulting from crushing or abrasion.	<ul> <li>Check tension on underlying layers. Bridon recommends an installation tension of between 2% and 10% of the minimum breaking force of the wire rope. Care should be taken to ensure that tension is retained in service. Insufficient tension will result in these lower layers being more prone to crushing damage.</li> </ul>
	<ul> <li>Review wire rope construction. Dyform wire ropes are more resistant to crushing on underlying layers than conventional rope constructions.</li> </ul>
	• Do not use more rope than necessary.
	Check drum diameter. Insufficient bending ratio increases tread pressure.

# Troubleshooting Guide

Problem
Wires looping from strands.
"Pigtail" or severe spiralling in rope.
Two single axial lines of broken wires running along the leng of the rope approximately 120 degrees apart indicating that the rope is being "nipped" in a tight sheave.
One line of broken wires running along the length of the rop indicating insufficient support for the rope, generally caused oversize sheave or drum grooving.
Short rope life resulting from evenly/randomly distributed b fatigue wire breaks caused by bending through the reeving system.
Fatigue induced wire breaks are characterised by flat ends of the broken wires.

#### Cause/Action

- Insufficient service dressing.
- Consider alternative rope construction.
- If wires are looping out of the rope underneath a crossover point, there may be insufficient tension on the lower wraps on the drum.
- Check for areas of rope crushing or distortion.
- Check that the sheave and drum diameter is large enough Bridon recommends a minimum ratio of rope/sheave to nominal drum diameter depending on the chosen construction, please contact Bridon for further reference.
- Indicates that the rope has run over a small radius or sharp edge.
- Check to see if the rope has "jumped off" a sheave and has run over a shaft.
- Check sheave and drum groove radii using sheave gauge to ensure that they are no smaller than nominal rope radius + 5% - Bridon would recommend that the sheave/drum groove radii are checked prior to any rope installation.
- Repair or replace drum/sheaves if necessary.
- Check to see if the groove diameter is no greater than 15% greater than the nominal rope diameter.
- Repair or replace drum/sheaves if necessary.
- Check for contact damage.
- Bending fatigue is accelerated as the load increases and as the bending radius decreases. Consider whether either factor can be improved.
- Check wire rope construction Dyform ropes are capable of doubling the bending fatigue life of a conventional steel wire rope.

# Troubleshooting Guide

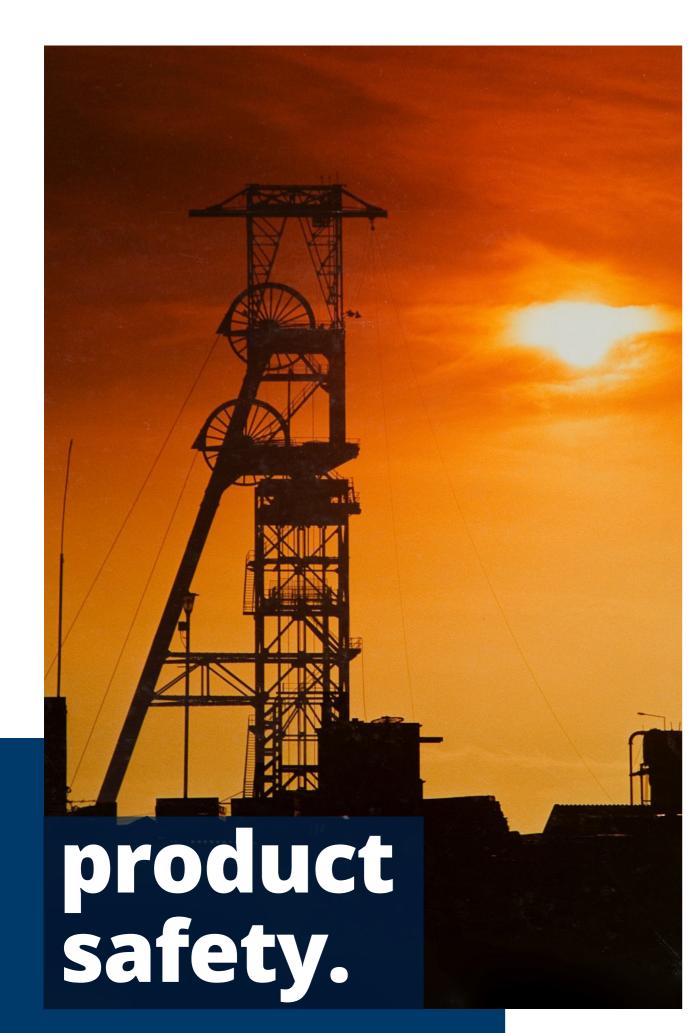
Problem	Cause/Action
Short rope life resulting from localised bend fatigue wire breaks. Fatique induced wire breaks are characterised by flat ends on the broken wires.	<ul> <li>Bending fatigue is accelerated as the load increases and as the bending radius decreases. Consider whether either factor can be improved.</li> <li>Check wire rope construction - Dyform ropes are capable of doubling the bending fatigue life of a conventional steel wire rope.</li> <li>Localised fatigue breaks indicate continuous repetitive bends over a short length. Consider whether it is economic to periodically shorten the rope in order to move the rope through the system and progressively expose fresh rope to the severe bending zone. In order to facilitate this procedure it may be necessary to begin operating with a slightly longer length of rope.</li> </ul>
Broken rope - ropes are likely to break when subjected to substantial overload or misuse particularly when a rope has already been subjected to mechanical damage. Corrosion of the rope both internally and/or externally can also result in a significant loss in metallic area. The rope strength is reduced to a level where it is unable to sustain the normal working load.	Review operating conditions.
Wave or corkscrew deformations normally associated with multi-strand ropes.	<ul> <li>Check sheave and drum groove radii using sheave gauge to ensure that they are no smaller than nominal rope radius +5% - Bridon recommends that the sheave/drum groove radii are checked prior to any rope installation.</li> <li>Repair or replace drum/sheaves if necessary.</li> <li>Check fleet angles in the reeving system - a fleet angle in excess of 1.5 degrees may cause distortion .</li> <li>Check that rope end has been secured in accordance with manufacturers instructions.</li> <li>Check operating conditions for induced turn.</li> <li>Good installation practices are vital to prevent torque build up in your new rope. Installation at 90 degrees to the main drum will add torque to all stranded/multi-strand ropes.</li> </ul>
Rotation of the load in a single fall system.	<ul><li> Review rope selection.</li><li> Consider use of rotation resistant or low rotation rope.</li></ul>
Rotation of the load in a multi - fall system resulting in "cabling" of the rope falls. Possibly due to induced turn during installation or operation.	<ul> <li>Review rope selection.</li> <li>Consider use of rotation resistant or low rotation rope.</li> <li>Review installation procedure or operating procedures.</li> </ul>
Core protrusion or broken core in single layer six or eight strand rope.	Caused by repetitive shock loading - review     operating conditions.

# Troubleshooting Guide

P	ope accumulating or "stacking" at drum flange - due to
	nsufficient fleet angle.
	unken wraps of rope on the drum normally associated wit nsufficient support from lower layers of rope or grooving.
S	hort rope life induced by excessive wear and abrasion.
E	xternal corrosion.
lr	nternal corrosion.

#### Cause/Action

- •Review drum design with original equipment manufacturer consider adding rope kicker, fleeting sheave etc.
- •Check correct rope diameter.
- ·If grooved drum check groove pitch.
- •Check tension on underlying layers Bridon recommend an installation tension of between 2% and 10% of the minimum breaking force of the wire rope - Care should be taken to ensure that tension is retained in service. Insufficient tension will result in these lower layers being more prone to crushing damage.
- •Make sure that the correct rope length is being used. Too much rope (which may not be necessary) may aggravate the problem.
- •Check fleet angle to drum.
- •Check general alignment of sheaves in the reeving system.
- •Check that all sheaves are free to rotate.
- •Review rope selection. The smooth surface of Dyform wire ropes gives better contact with drum and sheaves and offers improved resistance to "interference" between adjacent laps of rope.
- •Consider selection of galvanised rope.
- •Review level and type of service dressing.
- •Consider selection of galvanised rope.
- •Review frequency amount and type of service dressing.
- •Consider selection of plastic impregnated (PI) wire rope.



The following Instructions and Warnings combine to provide guidance on Product Safety and are intended for use by those already having a working knowledge of wire ropes, as well as the new user. They should be read, followed and passed on to others.

Failure to read, understand and follow these instructions could result in harmful and damaging consequences.

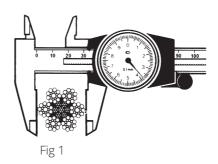
A 'Warning' statement indicates a potential hazardous situation which could result in a significant reduction in rope performance and/or put at risk, either directly or indirectly, the safety or health of those persons within the danger zone of the rope and its associated equipment.

Note: As a result of the creation of the single European market and the 'New Approach' Directives which set out 'essential requirements' (e.g. for safety); designers, manufacturers, suppliers, specifiers and users need to keep themselves abreast of any changes to the appropriate Regulations and national standards.

- 1. Storage
- 1.1 Unwrap the rope and examine the rope immediately after delivery to check its identification and condition and verify that it is in accordance with the details on the Certificates and/or other relevant documents.

Note: The rope should not be used for lifting purposes without the user having a valid Certificate in his possession.

Check the rope diameter and examine any rope terminations to ensure that they are compatible with the equipment or machinery to which they are to be fitted. (See Fig. 1)



waterproof material if the delivery site conditions preclude inside storage.

Rotate the reel periodically during long periods of storage, particularly in warm environments, to prevent migration of the lubricant from the rope.

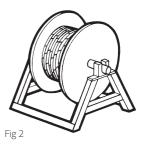
#### WARNING

Never store wire rope in areas subject to elevated temperatures as this may seriously affect its future performance. In extreme cases its original as-manufactured strength may be severely reduced rendering it unfit for safe use. Ensure that the rope does not make any direct contact with the floor and that there is a flow of air under the reel.

#### WARNING

Failure to do so may result in the rope becoming contaminated with foreign matter and start the onset of corrosion before the rope is even put to work.

Support the reel on a simple A-frame or cradle, located on ground which is capable of supporting the total mass of rope and reel. (See Fig. 2) Ensure that the rope is stored where it is not likely to be affected by chemical fumes, steam or other corrosive agents.



#### WARNING

Failure to do so may seriously affect its condition rendering it unfit for safe use.

1.3 Examine ropes in storage periodically and, when necessary, apply a suitable dressing which is compatible with the manufacturing lubricant. Contact the rope supplier, Bridon or original equipment manufacturer's (OEM) manual for guidance on types of dressings available, methods of application and equipment for the various types of ropes and applications.

Re-wrap the rope unless it is obvious that this will be detrimental to rope preservation. (Refer to the relevant Product Data sheets on rope dressings for more detailed information.)

#### WARNING

Failure to apply the correct dressing may render the original manufacturing lubricant ineffective and rope performance may be significantly affected.

Ensure that the rope is stored and protected in such a manner that it will not be exposed to any accidental damage either during the storage period or when placing the rope in, or taking it out of storage.

#### 🔥 WARNING

Failure to carry out or pay attention to any of the above could result in a loss of strength and/or a reduction in performance. In extreme cases the rope may be unfit for safe use.

2. Certification and Marking

Make sure that the relevant Certificate has been obtained before taking the rope into use for a lifting operation. (Refer to statutory requirements)

Check to verify that the marking on the rope or its package matches the relevant Certificate.

Note: The rating of a component part of a machine or lifting accessory is the responsibility of the designer of the machine or accessory. Any rerating of a lifting accessory must be approved by a competent person.

Retain the Certificate in a safe place for identification of the rope when carrying out subsequent periodic statutory examinations in service. (Refer to statutory requirements)

- 3. Handling and Installation
- 3.1 Handling and installation of the rope should be carried out in accordance with a detailed plan and should be supervised by a competent person.

#### 🛕 WARNING

Incorrectly supervised handling and installation procedures may result in serious injury to

persons in the vicinity of the operation as well as those persons directly involved in the handling and installation.

3.2 Wear suitable protective clothing such as overalls, industrial gloves, helmet, eye protectors and safety footwear (and respirator, particularly where the emission of fumes due to heat is likely).

#### 🛕 WARNING

Failure to wear suitable protective clothing and equipment may result in skin problems from over exposure to certain types of rope lubricants and dressings; burns from sparks, rope ends, molten lubricants and metals when cutting ropes or preparing sockets for re-use; respiratory or other internal problems from the inhalation of fumes when cutting ropes or preparing sockets for re-use; eye injuries from sparks when cutting ropes; lacerations to the body from wire and rope ends; bruising of the body and damage to limbs due to rope recoil, backlash and any sudden deviation from the line of path of rope.

- 3.3 Ensure that the correct rope has been supplied by checking to see that the description on the Certificate is in accordance with that specified in the purchaser's order.
- 3.4 Check by measurement that the nominal diameter of the new rope conforms to the nominal size stated on the Certificate.

For verification purposes, measure the diameter by using a suitable rope vernier fitted with jaws broad enough to cover not less than two adjacent strands. Take two sets of measurements spaced at least 1 metre apart, ensuring that they are taken at the largest cross-sectional dimension of the rope. At each point take measurements at right angles to each other.

The average of these four measurements should be within the tolerances specified in the appropriate Standard or Specification.

For a more general assessment of rope diameter use a rope calliper. (See Fig 1)

- 3.5 Examine the rope visually to ensure that no damage or obvious signs of deterioration have taken place during storage or transportation to the installation site.
- 3.6 Check the working area around the equipment for any potential hazards which may affect the safe installation of the rope.
- 3.7 Check the condition of the rope-related equipment in accordance with the OEM's instructions. Include the following -
- Sheave and Drum Sizes

Regulations throughout the world quote various minimum D:d ratios for differing rope constructions and these must be considered when selecting a suitable hoist rope. However as guidance the following D:d ratios are recommended.

6 Stranded ropes 80:1 Multi Stranded ropes 80:1 Locked coil ropes 100-120:1 depending upon rope diameter. (In addition the drum to outer wire ratio should be between 1000 and 1500:1)

Factors such as speed can necessitate an increase in the D:d ratio and in certain circumstances a D:d ratio below the recommended value can be tolerated but some reduction in rope life should be expected.

BRIDON's Mining Division will be pleased to advise on this subject.

#### Sheave Grooves

Groove diameters should be such that they can accommodate a new rope taking into account the relevant oversize tolerance and the fleet angles involved to provide adequate circumferential support.

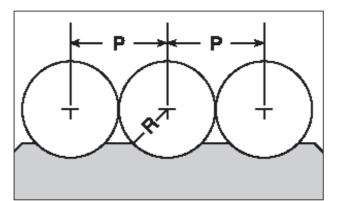
## Product Safety: Instructions & Warnings on the use of steel wire rope

A groove diameter of 7.5% greater than the nominal rope diameter is normally acceptable. However in certain cases experience has shown that clearances between 10 and 12.5% are required to obtain optimum performance.

Before installing a new rope all sheave grooves should be checked to ensure they provide the recommended clearance.

#### Drum Grooves

On single layer drum hoists spiral grooving is recommended. Where multi-layer coiling is necessary then parallel grooves or one of the patterned coiling systems should be used. In all cases correct pitch, clearance and groove depth are essential to obtain good rope performance.



Dimensions for grooving of drums

General recommendations for stranded ropes

P = nominal diameter + 5%

R = nominal radius + 7.5%

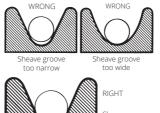
A gap between the last turn on the bottom layer of rope on the drum and the flange can be corrected by fitting a packing (or false cheek) of suitable thickness on the inside of the flange.

#### 🛕 WARNING

Failure to carry out any of the above could result in unsatisfactory and unsafe rope performance.

Note: Grooves must have clearance for the rope and provide adequate circumferential support to allow for free movement of the strands and facilitate bending. When grooves become worn and the rope is pinched at the sides, strand and wire movement is restricted and the ability of the rope to bend is reduced. (See Fig. 4)

Fig 4



Sheave groove correctly supporting the rope for 33% of its circumference When a new rope is fitted a variation in size compared with the old worn rope will be apparent. The new rope may not fit correctly into the previously worn groove profile and unnecessary wear and rope distortion is likely to occur. This may be remedied by machining out the grooves before the new rope is installed. Before carrying out such action the sheaves or drum should be examined to ensure that there will be sufficient strength remaining in the underlying material to safely support the rope.

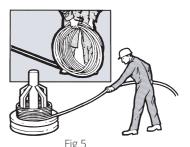
The competent person should be familiar with the requirements of the appropriate application/machinery standard.

Note: General guidance to users is given in ISO 4309 Code of practice for the selection, care and maintenance of steel wire rope.

Transfer the wire rope carefully from the storage area to the installation site.

#### Coils

Place the coil on the ground and roll it out straight ensuring that it does not become contaminated with dust/grit, moisture or any other harmful material. (See Fig. 5)



If the coil is too large to physically handle it may be placed on a 'swift' turntable and the outside end of the rope pulled out allowing the coil to rotate. (See Fig. 5)

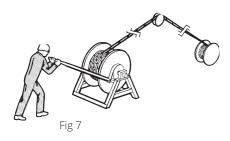
#### \rm MARNING

Never pull a rope away from a stationary coil as this will induce turn into the rope and kinks will form. These will adversely affect rope performance. (See Fig. 6)

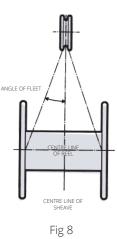


#### Reels

Pass a shaft through the reel and place the reel in a suitable stand which allows it to rotate and be braked to avoid overrun during installation. Where multi-layer coiling is involved it may be necessary for the reel to be placed in equipment which has the capability of providing a back tension in the rope as it is being transferred from reel to drum. This is to ensure that the underlying (and subsequent) laps are wound tightly on the drum. (See Fig. 7)



Position the reel and stand such that the fleet angle during installation is limited to 1.5 degrees. (See Fig. 8)



If a loop forms in the rope ensure that it does not tighten to form a kink.

#### <u> M</u>WARNING

A kink can severely affect the strength of a six strand rope and can result in distortion of a rotation- resistant or low rotation rope leading to its immediate discard. Ensure that the reel stand is mounted so as not to create a reverse bend during reeving (i.e. for a winch drum with an overlap rope, take the rope off the top of the reel). (See Fig. 7)

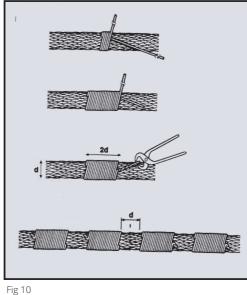
- 3.9 Ensure that any equipment or machinery to be roped is correctly and safely positioned and isolated from normal usage before installation commences. Refer to the OEM's instruction manual and the relevant 'Code of Practice'.
- 3.10 When releasing the outboard end of the rope from a reel or coil, ensure that this is done in a controlled manner. On release of the bindings and servings used for packaging, the rope will want to straighten itself from its previously bent position. Unless controlled, this could be a violent action. Stand clear.

A WARNING	
Failure to control could result in injury.	

# Product Safety: Instructions & Warnings on the use of steel wire rope

3.11 Monitor the rope carefully as it is being pulled into the system and make sure that it is not obstructed by any part of the structure or mechanism which may cause the rope to

come free.



#### \rm MARNING

Failure to monitor during this operation could result in injury.

This entire operation should be carried out carefully and slowly under the supervision of a competent person.

3.12 Take particular care and note the manufacturer's instructions when the rope is required to be cut. Apply secure servings on both sides of the cut mark. (See Fig. 10 for typical method of applying a serving to a multi-layer rope.)

Ensure that the length of serving is at least equal to two rope diameters. (Note: Special servings are required for spiral ropes, i.e. spiral strand and locked coil.) Length of serving for locked coil winding ropes and half locked coil guide ropes

The length of rope to be served depends on the object of the serving and on the size and type of the rope. If the serving is to restrain the cut end of a rope it must be longer than one intended to restrain the end of a short sample to be cut from a rope. A rope of the stranded type exerts only a moderate bursting force on a serving but a large locked coil rope exerts a considerable bursting force and, should the serving burst, the rope will unlay itself violently over a long length. Thus, for the cut end of a stranded rope, two servings each of a length at least six times the rope diameter should be used and kept in place until the rope end is otherwise secured. For the cut end of a large locked coil rope a serving or servings of each length of twenty times the rope diameter is advisable, (FLCWR's to be served with tinned annealed single wire serving, then secured by soldering these wires together, refer to Bridon for further technical information). The 'buried wire' with multi-strand serving wire should not be used with rotation resistant ropes. These servings should be backed up by a minimum of six two-bolt clamps set clear of the served length until the rope end is otherwise secured. Servings should be left permanently on locked coil winding ropes so that there is one about 0.6m (2ft) clear of the capel to allow proper examination of the rope at this point and another between the capel and the nearest pulley or driving sheave in the head frame. This is to localise any unlaying of the rope end, or of broken wires, in the event of an incident.

One serving either side of the cut is normally sufficient for preformed ropes. For non-preformed ropes, multi-layer (i.e. rotation-resistant and low rotation ropes) and parallel closed ropes (i.e. DSC ropes) a minimum of two servings each side of the cut will be necessary (See Fig. 10).

Arrange and position the rope in such a manner that at the completion of the cutting operation the rope ends will remain in position, thus avoiding any backlash or any other undesirable movement.

Cut the rope with a high speed abrasive disc cutter. Other suitable mechanical or hydraulic shearing equipment may be used although not recommended when a rope end is required to be welded or brazed.

For serving instructions for FL and HL ropes refer to Bridon.

#### 🔥 WARNING

When using a disc cutter be aware of the danger from sparks, disc fragmentation and fumes. (Refer 3.2.)

Ensure adequate ventilation to avoid any build-up of fumes from the rope and its constituent parts including any fibre core (natural or synthetic) any rope lubricant(s) and any synthetic filling and/or covering material.

#### \land WARNING

Some special ropes contain synthetic material which, when heated to a temperature higher than normal production processing temperatures, will decompose and may give off toxic fumes.

#### \land WARNING

Rope produced from carbon steel wires in the form shipped is not considered a health hazard. During subsequent processing (e.g. cutting, welding, grinding, cleaning) dust and fumes may be produced which contain elements which may affect exposed workers.

The products used in the manufacture of steel wire ropes for lubrication and protection present minimal hazard to the user in the form shipped. The user must however, take reasonable care to minimise skin and eye contact and also avoid breathing their vapour and mist.

After cutting, the rope cross-sections of nonpreformed ropes, multi-layer ropes and parallel closed ropes must be welded, brazed or fused and tapered such that all wires and strands in the rope are completely secured.

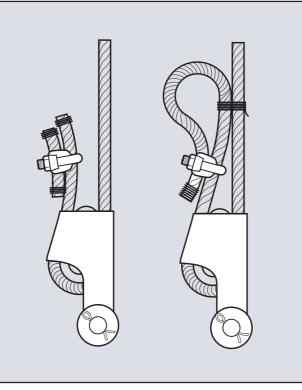
#### \rm MARNING

Failure to correctly secure the rope end is likely to lead to slackness, distortions, premature removal from service and a reduction in the breaking force of the rope.

3.13 Ensure that any fittings such as clamps or fixtures are clean and undamaged before securing rope ends.

Make sure that all fittings are secure in accordance with the OEM's instruction manual or manufacturer's instructions and take particular note of any specific safety requirements e.g. torque values (and frequency of any re-application of torque). When terminating a rope end with a wedge socket, ensure that the rope tail cannot withdraw through the socket by securing a clamp to the tail or by following the manufacturer's instructions.

(See Fig. 11 for two recommended methods of securing the rope tail of a wedge socket termination).



#### Fig 11

The loop back method uses a rope grip and the loop should be lashed to the live part of rope by a soft wire serving or tape to prevent flexing of the rope in service.

The method of looping back should not be used if there is a possibility of interference of the loop with the mechanism or structure.

#### \Lambda WARNING

Failure to secure in accordance with instructions could lead to loss of the rope and/or injury.

3.14 When coiling a rope on a plain (or smooth) barrel drum ensure that each lap lies tightly against the preceding lap. The application of tension in the rope greatly assists in the coiling of the rope.

# Product Safety: Instructions & Warnings on the use of steel wire rope

#### 🛕 WARNING

Any looseness or uneven winding will result in excessive wear, crushing and distortion of the rope.

With plain barrel drums it is difficult to achieve satisfactory multi-layer coiling beyond three layers.

The direction of coiling of the rope on the drum is important, particularly when using plain barrel drums, and should be related to the direction of lay of the rope in order to induce close coiling.

(See Fig. 12 for proper method of locating rope anchorage point on a plain drum.)

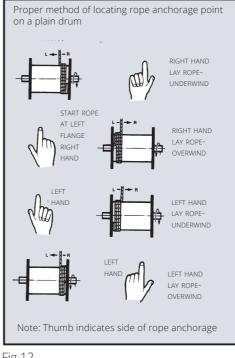


Fig 12

When multi-layer coiling has to be used it should be realised that after the first layer is wound on a drum, the rope has to cross the underlying rope in order to advance across the drum in the second layer. The points at which the turns in the upper layer cross those of the lower layer are known as the cross-over points and the rope in these areas is susceptible to increased abrasion and crushing. Care should be taken when installing a rope on a drum and when operating a machine to ensure that the rope is coiled and layered correctly.

 3.15 Check the state of re-usable rope end terminations for size, strength, defects and cleanliness before use.
 Non-destructive testing may be required depending on the material and circumstances of use. Ensure that the termination is fitted in accordance with the OEM's instruction manual or manufacturer's instructions.

When re-using a socket and depending on its type and dimensions, the existing cone should be pressed out. Otherwise, heat may be necessary.

#### 🛕 WARNING

When melting out sockets which have previously been filled with hot metal, the emission of toxic fumes is likely. Note that white metal contains a high proportion of lead.

Correctly locate and secure any connection pins and fittings when assembling end terminations to fixtures. Refer to manufacturer's instructions.

#### \rm MARNING

Failure to pay attention to any of the above could result in unsafe operation and potential injury.

- 3.16 Limit switches, if fitted, must be checked and re-adjusted, if necessary, after the rope has been installed.
- 3.17 Record the following details on the Certificate after installation has been completed: type of equipment, location, plant reference number, duty and date of installation and any re-rating information/signature of competent person. Then safely file the Certificate.
- 3.18 'Run in' the new rope by operating the equipment slowly, preferably with a low load, for several cycles. This permits the new rope to adjust itself gradually to working conditions.

Note: Unless otherwise required by a certifying authority, the rope should be in this condition before any proof test of the equipment or machinery is carried out.

Check that the new rope is spooling correctly on the drum and that no slack or cross laps develop.

If necessary, apply as much tension as possible to ensure tight and even coiling, especially on the first layer.

Where multi-layer coiling is unavoidable, succeeding layers should coil evenly on the preceding layers of rope.

#### \rm MARNING

Irregular coiling usually results in severe surface wear and rope malformation, which in turn is likely to cause premature rope failure.

- 3.19 Ensure that the as-manufactured condition of the rope is maintained throughout the whole of the handling and installation operation.
- 3.20 If samples are required to be taken from the rope for subsequent testing and/or evaluation, it is essential that the condition of the rope is not disturbed. Refer to the instructions given in 3.12 and, depending on the rope type and construction, any other special manufacturer's instructions.
- 4. In Service
- 4.1 Inspect the rope and related equipment at the beginning of every work period and particularly following any incident which could have damaged the rope or installation.

The entire length of rope should be inspected and particular attention paid to those sections that experience has proven to be the main areas of deterioration. Excessive wear, broken wires, distortion and corrosion are the usual signs of deterioration. For a more detailed examination special tools are necessary (see Fig. 13) which will also facilitate internal inspection (see Fig. 14.)



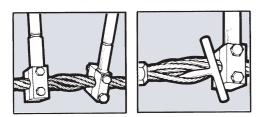


Fig 14

In the case of ropes working over drums or sheaves it is particularly necessary to examine those areas entering or leaving the grooves when maximum loads (i.e. shock loads) are experienced, or those areas which remain for long periods in exposed places such as over a head gear pulleys.

On some running ropes, but particularly relevant to standing ropes (e.g. guide ropes) the areas adjacent to terminations should be given special attention (see Fig. 14). Note: Shortening the rope re-positions the areas of maximum deterioration in the system. Where conditions permit, begin operating with a rope which has a slightly longer length than necessary in order to allow for periodic shortening.

When a non-preformed rope, multi-layer rope or parallel closed rope is used with a wedge socket and is required to be shortened, it is essential that the end of the rope is secured by welding or brazing before the rope is pulled through the main body of the socket to its new position. Slacken the wedge in the socket. Pass the rope through the socket by an amount equivalent to the crop length or sample required. Note that the original bent portion of the rope must not be retained within the wedge socket. Replace the wedge and pull up the socket. Prepare and cut in accordance with section 3.12. Ensure that the rope tail cannot withdraw through the socket, see section 3.13.

#### \rm MARNING

Failure to observe this instruction will result in a significant deterioration in the performance of the rope and could render the rope completely unfit for further service.

In cases where severe rope wear takes place at one end of a wire rope, the life of the rope may be extended by changing round the drum end with the load end, i.e. turning the rope 'end for end' before deterioration becomes excessive.

4.2 Remove broken wires as they occur by bending backwards and forwards using a pair of pliers until they break deep in the valley between two outer strands (see Fig. 15). Wear protective clothing such as overalls, industrial gloves, helmet, eye protectors and safety footwear during this

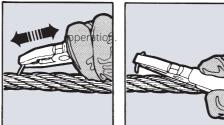


Fig 15

#### \rm MARNING

Do not shear off the ends of broken wires with pliers as this will leave an exposed jagged edge which is likely to damage other wires in the rope and lead to premature removal of the rope from service. Failure to wear adequate protective clothing could result in injury.

## Product Safety: Instructions & Warnings on the use of steel wire rope

Note: Broken wires are a normal feature of service, more so towards the end of the rope's life, resulting from bending fatigue and wear. The local break up of wires may indicate some mechanical fault in the equipment.

Record the number and position in the rope of any removed broken wires.

- 4.3 Do not operate an appliance if for any reason (e.g. rope diameter, certified breaking force, rope construction, length or strength and type of rope termination) the wire rope and its termination is considered unsuitable for the required duty.
- 4.4 Do not operate an appliance if the wire rope fitted has become distorted, been damaged or has deteriorated to a level such that discard criteria has been reached or is likely to be reached prior to normal expected life based on historical performance data.

#### 🛕 WARNING

Rope distortion is usually a result of mechanical damage and can significantly reduce rope strength.

- 4.5 An authorised competent person must examine the rope in accordance with the appropriate Regulations.
- 4.6 Do not carry out any inspection, examination, dressing/ lubrication, adjustment or any other maintenance of the rope whilst it is suspending a load, unless otherwise stated in the OEM's instruction manual or other relevant documents.

Do not carry out any inspection or maintenance of the rope if the appliance controls are unattended unless the surrounding area has been isolated or sufficient warning signs have been posted within the immediate vicinity.

If the appliance controls are attended, the authorised person must be able to communicate effectively with the driver or controller of the appliance during the inspection process.

4.7 Never clean the wire rope without recognising the potential hazards associated with working on a moving rope.

#### \land WARNING

Failure to pay attention or take adequate precaution could result in injury.

If cleaning by cloth/waste, the material can be snagged on damaged surfaces and/or broken wires. If cleaning by brush, eye protectors must be worn. If using fluids it should be recognised that some products are highly inflammable. A respirator should be worn if cleaning by a pressurised spray system.

#### \rm MARNING

Failure to take adequate precaution could result in injury or damage to health.

Only use compatible cleaning fluids which will not impair the original rope lubricant nor affect the rope associated equipment.

#### \rm MARNING

The use of cleaning fluids (particularly solvent based) is likely to 'cut back' the existing rope lubricant leading to a greater quantity of lubricant accumulating on the surface of the rope. This may create a hazard in appliances and machinery which rely on friction between the rope and the drive sheave (e.g. lifts, friction winders and cableways).

4.8 Lubricants selected for in-service dressing must be compatible with the rope manufacturing lubricant and should be referenced in the OEM's instruction manual or other documents approved by the owner of the appliance.

If in doubt contact the rope supplier or Bridon.

4.9 Take particular care when applying any in-service lubricant/ dressing. Application systems which involve pressure should only be operated by trained and authorised persons and the operation carried out strictly in accordance with the manufacturer's instructions.

Most wire ropes should be lubricated as soon as they are put into service and at regular intervals thereafter (including cleaning) in order to extend safe performance.

#### 🛕 WARNING

A 'dry' rope unaffected by corrosion but subject to bend fatigue, is likely to achieve only 30% of that normally attained by a 'lubricated' rope.

Do not dress/lubricate the rope if the application required it to remain dry. (Refer OEM's instruction manual.)

Reduce the period between examinations when ropes are not subjected to any in-service dressing and when they must remain dry.

Note: The authorised person carrying out a rope inspection must be capable of recognising the potential loss of safe performance of such a rope in comparison with lubricated rope.

Clean the rope before applying a fresh dressing/lubricant if it is heavily loaded with foreign matter e.g. sand, dust.

4.10 The authorised person responsible for carrying out wire rope maintenance must ensure that the ends of the rope are secure. At the drum end this will involve checking the integrity of the anchorage and ensuring that there are at least two and a half dead laps tightly coiled. At the outboard end the integrity of the termination must be checked to ensure that it is in accordance with the OEM's manual or other documents approved by the owner of the appliance.

Adjust the lengths of ropes in multi-rope systems in order that equal forces (within approved limits) are evident.

If a wire rope needs cutting refer to 3.12.

When securing rope ends refer to 3.13.

When re-usable end terminations are used refer to 3.15.

When re-connecting any end terminations to fixtures refer to 3.15.

#### \rm MARNING

Damage to, or removal of component parts (mechanical or structural) caused by abnormal contact with wire rope can be hazardous to the safety of the appliance and/or the performance of the rope (e.g. damage to the drum grooving, such that coiling is erratic and/or the rope is 'pulled down' into underlying layers, which might cause a dangerous condition or, alternatively, cause localised rope damage at 'cross-over' positions, which might then radically affect performance; loss/ removal of wear plates protecting the structure leading to major structural damage by cutting and/or failure of the wire rope due to mechanical severance).

- 4.12 Following any periodic statutory examination or routine or special inspection where any corrective action is taken the Certificate should be updated and a record made of the defects found, the extent of the changes and the condition of the rope.
- 4.13 Apply the following procedures for the selection and preparation of samples, from new and used lengths of rope, for the purpose of examination and testing to destruction.

Check that the rope end, from which the sample will be taken, is secured by welding or brazing. If not, select the sample length further away from the rope end and prepare new servings (see 3.12).

Handle the rope in accordance with the instructions given in section 3. Serve the rope, using the buried wire technique (see Fig. 10) and apply a rope clamp or grip as

close to the cut mark as practically possible. Do not use solder to secure the servings.

Ensure that the sample is kept straight throughout the whole procedure and ensure that the minimum sample length is 3 metres for ropes up to and including 40mm diameter and 12 metres for larger diameter ropes.

The rope should be cut with a high speed abrasive disc cutter or an oxyacetylene torch. Weld the rope ends of the sample as described in section 3.12, after which the clamp or grip can be removed.

The identification of the rope must be established and the sample suitably marked and packed. It is recommended that the 3 metre sample is retained straight and secured to a wood batten for transportation. For a 12 metre sample, coil to a diameter as large as practically possible and never less than 2 metres.

Note: Samples taken for destruction testing are required to be terminated in accordance with a recognised resin socketing standard (e.g. BS EN 13411-4 or ISO 7596).

#### 🛕 WARNING

Failure to comply with these procedures will result in measured breaking force values which are not truly representative of the actual strength of the rope.

- 5. Wire Rope Discard
- 5.1 Discard the wire rope in accordance with current Regulations and in accordance with the OEM's instruction manual.
- 5.2 If a wire rope is removed from service at a level of performance substantially different to historically established performance data and without any obvious reason(s), contact Bridon or Bridon's distributor for further guidance.
- 5.3 Only qualified and experienced personnel, taking the appropriate safety precautions and wearing the appropriate protective clothing, should be responsible for removing the wire rope.

#### \rm MARNING

Take particular care when removing ropes with mechanical damage as they may fail abruptly during the change-out procedure.

## Product Safety: Instructions & Warnings on the use of steel wire rope

Take the utmost care when removing 'exhausted/failed' ropes from drums and sheaves as they may be grossly distorted, lively and tightly coiled.

#### \land WARNING

Failure to take adequate precautions could result in injury.

5.4 Store discarded rope in a safe and secure location or compound and ensure that it is suitably marked to identify it as rope which has been removed from service and not to be used again.

#### 🛕 WARNING

Discarded rope can be a danger (e.g. protruding broken wires, excessive grease/lubricant and rope mass) to personnel and equipment if not handled correctly and safely during disposal.

- 5.5 Record the date and reason for discard on the Certificate before filing for future reference.
- 5.6 Pay attention to any Regulations affecting the safe disposal of steel wire rope.
- 6. Rope Selection Criteria

Ensure that the correct type of wire rope is selected for the equipment by referring to the OEM's instruction manual or other relevant documents. If in doubt contact Bridon or Bridon's distributor for guidance.

6.1 Rope Strength

If necessary, refer to the appropriate Regulations and/or application standards and calculate the maximum force to which the rope will be subjected.

The calculation may take into account the mass to be lifted or moved, any shock loading, effects of high speed, acceleration, any sudden starts or stops, frequency of operation and sheave bearing friction.

By applying the relevant coefficient of utilisation (safety factor) and, where applicable, the efficiency of the rope termination, the required minimum breaking load or force of the rope will be determined, the values of which are available from the relevant National, European or International standards or from specific Product Data literature. If in doubt ask for advice from Bridon or Bridon's distributor.

6.2 Bending fatigue

The size and number of sheaves in the system will influence the performance of the rope.

#### 🛕 WARNING

Wire rope which bends around sheaves, rollers or drum will deteriorate through 'bending fatigue'. Reverse bending and high speed will accelerate the process. Therefore, under such conditions select a rope with high bending fatigue resistance. Refer to Product Data Information, and if in doubt ask for advice.

#### 6.3 Abrasion

Wire rope which is subject to abrasion will become progressively weaker as a result of:

Externally - dragging it through overburden, sand or other abrasive materials and passing around a sheave, roller or drum.

#### WARNING

Abrasion weakens the rope by removing metal from both the inner and outer wires. Therefore, a rope with large outer wires should normally be selected.

#### 6.4 Vibration

Vibration in wire rope will cause deterioration. This may become apparent in the form of wire fractures where the vibration is absorbed.

#### \rm MARNING

These fractures may be internal only and will not be visually identified.

#### 6.5 Distortion

Wire rope can be distorted due to high pressure against a sheave, improperly sized grooves or as a result of multilayer coiling on a drum.

Rope with a steel core is more resistant to crushing and distortion.

#### 6.6 Corrosion

Rope with a large number of small wires is more susceptible to corrosion than rope with a small number of large wires. Therefore, if corrosion is expected to have a significant effect on rope performance select a galvanised rope with as large an outer wire size as possible bearing in mind the other conditions (e.g. bending and abrasion) under which the rope will be operating.

6.7 Connecting Ropes

In the event that it is necessary to connect one rope to another (in series) it is essential that they have the required strength, are of the same type and both have the same lay direction (i.e. connect 'right' lay to 'right' lay).

#### \land WARNING

Failure to heed this warning could result in catastrophic failure particularly at a termination which is capable of being pulled apart (i.e. splice) due to unlaying.

#### 6.8 Rope Length

Rope length and /or difference in length between two or more ropes used in a set may be a critical factor and must be considered along with rope selection.

#### 🛕 WARNING

Wire rope will elongate under load. Other factors such as temperature, rope rotation and internal wear will also have an effect. These factors should also be considered during rope selection.

#### 6.9 Preformed and Non-preformed Ropes

Single layer round strand rope is normally supplied preformed. However, if a non-preformed rope is selected then personnel responsible for its installation and/or maintenance need to take particular care when handling such rope, especially when cutting. For the purposes of this instruction, multi-layer, parallel closed and spiral ropes should be regarded as non-preformed ropes.

#### 6.10 Operating Temperatures

Wire rope with a steel core should be selected if there is any evidence to suggest that a fibre core will not provide adequate support to the outer strands and/or if the temperature of the working environment may be expected to exceed 100°C.

For operating temperatures above 100°C de-rating of the minimum breaking force of the rope is necessary (e.g. between 100°C and 200°C reduce by 10%; between 200°C and 300°C reduce by 25%; between 300°C and 400°C reduce by 35%).

Do not use ropes with high carbon wires above 400 °C.

#### 🛕 WARNING

Failure to observe this general guidance could result in failure of the ropes to support the load.

For temperatures over 400°C, other materials such as stainless steel or other special alloys should be considered.

#### 🛕 WARNING

Rope lubricants and any synthetic filling and/or covering materials may become ineffective at certain low or high operating temperature levels.

Certain types of rope end terminations also have limiting operating temperatures and the manufacturer or Bridon should be consulted where there is any doubt. Ropes with aluminium ferrules must not be used at temperatures in excess of 150 °C.

# Product Safety: Instructions & Warnings on the use of steel wire rope

#### 🛕 WARNING

CAUTIONARY NOTICE – RESTRICTIONS ON THE USE OF LARGE DIAMETER MULTI-STRAND ROPES.

All wire ropes are prone to damage if they are not properly supported when used at high loads. Larger Multi-strand ropes are particularly susceptible to this form of abuse, due to their rigid construction and the relatively fine wire sizes involved in their manufacture/construction. Instances have been recorded of ropes being heavily worked over plain drums and failing "prematurely", despite the nominal tension being

Type of contact	Close-fitting U-groove	Oversize U-groove	Plain drum
Level of support	Good	Fair	Poor
Tread path width	100% of rope dia.	50% of rope dia.	20% of rope dia.
Tread pressure =	2T/Dd	4T/Dd	10T/Dd
Contact stress =	20T/Dd	40T/Dd	100T/Dd

Note: Contact stresses which exceed 10% of the wire UTS should be considered a cause for concern, especially if the rope is operating at a low factor of safety.

[* This is because the true contact area is very much less than the projected nominal area.]

being in the region of half the breaking strength of the rope.

The best way of preventing difficulties of this sort is to avoid conditions that are likely to generate damagingly high contact stresses. A simple method of assessing the severity of the contact conditions is to firstly calculate the tread pressure based on the projected nominal area and then apply a factor (of say 10*) to allow for the highly localised and intermittent nature of the actual wire contacts, as indicated below :-

Worked example:

Consider case of a 50mm Multi-strand rope (MBL=2100kN) operating at a 3:1 factor of safety. Then, for the Contact stress < 200 Mpa say, the following minimum bending diameters are indicated:

Close-fitting groove – 1400mm Oversize U-groove – 2800mm Un-grooved drum – 7000mm

# Material Safety Data

#### Introduction

Steel wire rope is a composite material and dependent upon its type may contain a number of discrete materials. The following provides full details of all the individual materials which may form part of the finished wire rope.

The description and/or designation of the wire rope stated on the delivery note and/or invoice (or certificate, when applicable) will enable identification of the component parts.

The main component of a steel wire rope is the wire, which may be carbon steel, coated (zinc or Zn95/A15) steel or stainless steel.

The other three components are (i) the core, which may be of steel of the same type as used in the main strands or alternatively fibre (either natural or synthetic), (ii) the rope lubricant and, where applicable, (iii) any internal filling or external covering. No Occupational Exposure Limits (OEL's) exist for steel wire rope and the values provided in this publication relate to component elements and compounds. The actual figures quoted in relation to the component parts are taken from the latest edition of EH40.

Rope produced from carbon, coated or stainless steel wires in the as-supplied condition is not considered a health hazard. However during any subsequent processing such as cutting, welding, grinding and cleaning, dust and fumes may be produced which contain elements that may affect exposed workers.

The following indicates the order in which specific information is provided:-

Carbon steel wire, Coated steel wire, Stainless steel wire, Manufacturing rope lubricants, Fibre cores,

Carbon Steel Wire - Hazardous Ingredients				
Component	% Weight (Max)	Long term exposure limit (8-hour TWA reference period) mg/m ³	Short term exposure limit (10-minute reference period) mg/m ³	
BASE METAL				
Aluminium	0.3	10	20	
Carbon	1.0	None Listed		
Chromium	0.4	0.5		
Cobalt	0.3	0.1		
Copper	0.5	0.2		
Iron	Balance	5	10	
Manganese	1.0	5	5	
Molybdenum	0.1	5	10	
Nickel	0.5	1		
Phosphorus	0.1	0.1	0.3	
Silicon	0.5	10		
Sulphur	0.5	None Listed		
Vanadium	0.25	0.5		
Boron	0.1	10	20	
Titanium	0.1	10		
Nitrogen	0.01	5	9	
Lead	0.1	0.15		
Arsenic	0.01	0.2		
Zirconium	0.05	5	10	
COATED				
Sodium	0.5	None Listed		
Calcium	0.5	2		
Boron	1.0	10	20	
Phosphorus	1.0	0.1	0.3	
Iron	1.0	5	10	
Zinc	1.0	5	10	
Oil may be applied	5.0	5	10	

#### Physical Data

Specific Gravity:	7.5 - 8.5	Vapour Pressure:	N/A
Melting Point:	1350 - 1500 ∘C	Vapour Density:	N/A
Appearance & Odour:	Solid. Odourless Metal	Evaporation:	N/A
Solubility in water:	Insoluble	% Volatiles:	N/A
Flash Point:	None	Boiling Point:	> 2800 °C

# Material Safety Data

Coated (Zinc and ZN95/A 15) Steel Wire - Hazardous Ingredients

Component	% Weight (Max)	Long term exposure limit (8-hour TWA reference period) mg/m ³	Short term exposure limit (10-minute reference period) mg/m³
BASE METAL			
Aluminium	0.3	10	20
Carbon	1.0	None Listed	
Chromium	0.4	0.5	
Cobalt	0.3	0.1	
Copper	0.5	0.2	
Iron	Balance	5	10
Manganese	1.0	5	5
Molybdenum	0.1	5	10
Nickel	0.5	1	
Phosphorus	0.1	0.1	0.3
Silicon	0.5	10	
Sulphur	0.5	None Listed	
Vanadium	0.25	0.5	
Boron	0.1	10	20
Titanium	0.1	10	
Nitrogen	0.01	5	9
Lead	0.1	0.15	
Arsenic	0.01	0.2	
Zirconium	0.05	5	10
COATED			
Zinc	10.0	5	10
Aluminium	1.5	10	20
Iron	5.0	5	10
Sodium	0.5	None Listed	
Calcium	0.5	2	
Boron	1.0	100	20
Phosphorus	1.0	0.1	0.3
Sulphur	0.5	None Listed	
Oil may be applied	5.0	5	10
Wax may be applied	5.0	2	6

#### Physical Data

Specific Gravity:	7.5 - 8.5
Melting Point:	1350 - 1500 °C
Appearance & Odour:	Solid. Odourless Metal
Solubility in water:	Insoluble
Flash Point:	None
Flash Point:	None

Vapour Pressure:	N/A
Vapour Density:	N/A
Evaporation:	N/A
% Volatiles:	N/A
Boiling Point:	> 2800 °C

# Material Safety Data

#### Manufacturing Rope Lubricants

The products used in the manufacture of steel wire ropes for lubrication and protection present minimal hazard to the user in the as-supplied condition. The user must, however, take reasonable care to minimise skin and eye contact and also avoid breathing their vapours and mists.

A wide range of compounds is used as lubricants in the manufacture of steel wire rope. These products, in the main, consist of mixtures of oils, waxes, bitumens, resins, gelling agents and fillers with minor concentrations of corrosion inhibitors, oxidation stabilizers and tackiness additives.

Most of them are solid at ambient temperatures and provided skin contact with the fluid types is avoided, none present a hazard in normal rope usage.

However, to assist in the assessment of the hazard caused by these products, the following table contains all the components which may be incorporated into a wire rope lubricant and which may be considered hazardous to health.

#### Hazardous Ingredients:

Component	Long term exposure limit (8-hour TWA reference period) mg/m ³	Short term exposure limit (10-minute reference period) mg/m ³
Oil mist	5	10
Paraffin wax fume	2	6
Bitumen	5	10
Silica, fused		
Total inhalable	0.3	
dust	0.1	
Respirable dust	10	20
Aluminium flake	5	10
Zinc oxide, fume	1430	1780

There are no other known constituents of any wire rope lubricant used that are classified as hazardous in the current edition of EH40.

General advice on handling ropes with lubricants

To avoid the possibility of skin disorders, repeated or prolonged contact with mineral or synthetic hydrocarbons must be avoided and it is essential that all persons who come into contact with such products maintain high standards of personal hygiene.

The worker should:

- 1) use oil impermeable gloves, or if not available, suitable oil repellent type barrier creams,
- 2) avoid unnecessary contact with oil using protective clothing,
- 3) obtain first aid treatment for any injury, however slight,
- wash hands thoroughly before meals, before using the toilet and after work,

#### 5) use conditioning creams after washing, where provided.

- The worker should not:
- 1) put oily rags or tools into pockets, especially trousers,
- 2) use dirty or spoiled rags for wiping oil from the skin,
- 3) wear oil soaked clothing,
- 4) use solvents such as paraffin, petrol etc., to remove oil from the skin.

Concentrations of oil mists, fumes and vapours in the working atmosphere must be kept as low as is reasonably practicable. Levels quoted in the current edition of HSE Guidance Note EH40 'Occupational Exposure Limits' must not be exceeded.

#### Health Hazards

Inhalation of oil mists or fumes from heated rope lubricants in high concentrations may result in dizziness, headache, respiratory irritation or unconsciousness. Eye contact may produce mild transient irritation to some users.

Fumes from heated rope lubricants in high concentrations may cause eye irritation.

If heated rope lubricants contacts skin, severe burns may result.

Prolonged or repeated skin contact may cause irritation, dermatitis or more serious skin disorders.

#### Fibre Cores

Being in the centre of a steel wire rope, the materials (natural or synthetic) from which fibre cores are produced do not present a health hazard during normal rope handling. Even when the outer core strands are removed (for example when the rope is required to be socketed) the core materials present virtually no hazard to the users, except, maybe, in the case of a used rope where, in the absence of any service dressing or as a result of heavy working causing internal abrasive wear of the core, the core may have decomposed into a fibre dust which might be inhaled, although this is considered extremely unlikely.

The principal area of hazard is through the inhalation of fumes generated by heat, for example when the rope is being cut by a disc cutter.

# Material Safety Data

Under these conditions, natural fibres are likely to yield carbon dioxide, water and ash, whereas synthetic materials are likely to yield toxic fumes.

The treatment of natural fibres, such as rotproofing, may also produce toxic fumes on burning.

The concentrations of toxic fumes from the cores, however, will be almost negligible compared with the products generated by heating from the other primary materials, e.g. wire and manufacturing lubricant in the rope.

The most common synthetic core material is polypropylene, although other polymers such as polyethylene and nylon may occasionally be used.

#### Filling and Covering Materials

Filling and covering materials do not present a health hazard during handling of the rope in its as-supplied condition.

The principal area of hazard is by the inhalation of fumes generated by heat, for example when the rope is being cut by a disc cutter.

Under these conditions, fillings and coverings, which are generally polypropylene, polyethylene and polyamide (but in some cases may be of natural fibre) are likely to produce toxic fumes.

#### General Information

Occupational protective measures

- Respiratory protection Use general and local exhaust ventilation to keep airborne dust or fumes below established occupational exposure standards (OES's). Operators should wear approved dust and fume respirators if OES's are exceeded. (The OES for total dust is 10mg/m3 and for respirable dust is 5mg/m³).
- Protective equipment Protective equipment should be worn during operations creating eye hazards. A welding hood should be worn when welding or burning. Use gloves and other protective equipment when required.

3) Other - Principles of good personal hygiene should be followed prior to changing into street clothing or eating. Food should not be consumed in the working environment.

#### Emergency medical procedures

- 1) Inhalation Remove to fresh air; get medical attention.
- 2) Skin Wash areas well with soap and water.
- 3) Eyes Flush well with running water to remove particulate; get medical attention.
- 4) Ingestion In the unlikely event that quantities of rope or any of its components are ingested, get medical attention.

Safety Information

- Fire and explosion In the solid state, steel components of the rope present no fire or explosion hazard. the organic elements present, i.e. lubricants, natural and synthetic fibres and other natural or synthetic filling and covering materials are capable of supporting fire.
- 2) Reactivity Stable under normal conditions.

Spill or leak procedures

- 1) Spill or leak Not applicable to steel in the solid form.
- 2) Disposal Dispose of in accordance with local Regulations.

# Rope Terminology

#### Wires

Outer wires: All wires positioned in the outer layer of wires in a spiral rope or in the outer layer of wires in the outer strands of a stranded rope.

Inner wires: All wires of intermediate layers positioned between the centre wire and outer layer of wires in a spiral rope or all other wires except centre, filler, core and outer wires of a stranded rope.

Core wires: All wires of the core of a stranded rope.

Centre wires: Wires positioned either at the centre of a spiral rope or at the centres of strands of a stranded rope.

Layer of wires: An assembly of wires having one pitch circle diameter. The exception is Warrington layer comprising alternately laid large and small wires where the smaller wires are positioned on a larger pitch circle diameter than the larger wires. The first layer is that which is laid immediately over the strand centre.

Note: Filler wires do not constitute a separate layer.

Tensile strength grade of wires: A level of requirement of tensile strength of a wire and its corresponding tensile strength range. It is designated by the value according to the lower limit of tensile strength and is used when specifying wire and when determining the calculated minimum breaking force or calculated minimum aggregate breaking force of a rope.

Wire finish: The condition of the surface finish of a wire, e.g. bright, zinc coated.

# rope terminology.



# Rope Terminology

#### Strands

Strand: An element of rope usually consisting of an assembly of wires of appropriate shape and dimensions laid helically in the same direction in one or more layers around a centre.

Note: Strands containing three or four wires in the first layer or certain shaped (e.g. ribbon) strands may not have a centre.

Round strand: A strand with a cross-section which is approximately the shape of a circle.

Triangular strand: A strand with a cross-section which is approximately the shape of a triangle.

Note: Triangular strands may have built-up centres (i.e. more than one wire forming a triangle).

Oval strand: A strand with a cross-section which is approximately the shape of an oval

Flat ribbon strand: A strand without a centre wire with a crosssection which is approximately the shape of a rectangle.

Compacted strand: A strand which has been subjected to a compacting process such as drawing, rolling or swaging whereby the metallic cross-sectional area of the wires remains unaltered and the shape of the wires and the dimensions of the strand are modified.

Note: Bridon's brands of Dyform rope contain strands which have been compacted.

Single lay strand: Strand which contains only one layer of wires, e.g. 6-1.

Parallel lay strand: Strand which contains at least two layers of wires, all of which are laid in one operation (in the same direction), e.g. 9-9-1; 12-6F-6-1; 14-7+7-7-1. Each layer of wires lies in the interstices of the underlying layer such that they are parallel to one another, resulting in linear contact.

Note: This is also referred to as equal lay. The lay length of all the wire layers are equal.

Seale: Parallel lay strand construction with the same number of wires in each wire layer, each wire layer containing wires of the same size, e.g. 7-7-1; 8-8-1; 9-9-1.

Warrington: Parallel lay strand construction having an outer layer of wires containing alternately large and small wires, the number of wires in the outer layer being twice that in the underlying layer of wires, e.g. 6+6-6-1; 7+7-7-1.

Filler: Parallel lay strand construction having an outer layer of wires containing twice the number of wires than in the inner layer with filler wires laid in the interstices wires of the underlying layer of wires, e.g. 12-6F-6-1; 14-7F-7-1.

Combined parallel lay: Parallel lay strand construction having three or more layers of wires, e.g. 14-7+7-7-1; 16-8+8-8-1; 14-14-7F-7-1; 16-16-8F+8-1.

Note: The first two examples above are also referred to as Warrington-Seale construction. The latter two examples are also referred to as Seale-Filler construction. Multiple operation lay strand: Strand construction containing at least two layers of wires, at least one of which is laid in a separate operation. All of the wires are laid in the same direction.

Cross-lay: Multiple operation strand construction in which the wires of superimposed wire layers cross over one another and make point contact, e.g. 12/6-1.

Compound lay: Multiple operation strand which contains a minimum of three layers of wires, the outer layer of which is laid over a parallel lay centre, e.g. 16/6+6-6-1.

#### Ropes

Spiral Rope: An assembly of two or more layers of shaped and/ or round wires laid helically over a centre, usually a single round wire. There are three categories of spiral rope, viz. spiral strand, half-locked coil and full-locked coil.

Spiral Strand: An assembly of two or more layers of round wires laid helically over a centre, usually a single round wire.

Half-locked Coil Rope: A spiral rope type having an outer layer of wires containing alternate half lock and round wires.

Full-locked Coil Rope: A spiral rope type having an outer layer of full lock wires.

Stranded Rope: An assembly of several strands laid helically in one or more layers around a core or centre. There are three categories of stranded rope, viz. single layer, multi-layer and parallel-closed.

Single Layer Rope: Stranded rope consisting of one layer of strands laid helically over a core.

Note: Stranded ropes consisting of three or four outer strands may, or may not, have a core. Some three and four strand single layer ropes are designed to generate torque levels equivalent to those generated by rotation-resistant and low rotation ropes.

Rotation-resistant Rope: Stranded rope having no less than ten outer strands and comprising an assembly of at least two layers of strands laid over a centre, the direction of lay of the outer strands being opposite (i.e. contra - lay) to that of the underlying layer of strands.

Low Rotation Rope: Rotation resistant rope having at least fifteen outer strands and comprising an assembly of at least three layers of strands laid over a centre in two operations.

Note: this category of rotation resistant rope is constructed in such a manner that it displays little or no tendency to rotate, or if guided, generates little or no torque when loaded.

# Rope Terminology

Compacted Strand Rope: Rope in which the outer strands, prior to closing of the rope, are subjected to a compacting process such as drawing, rolling or swaging.

Note: Bridon's products containing compacted strands are identified by "Dyform".

Compacted Rope: Rope which is subjected to a compacting process after closing, thus reducing its diameter.

Solid Polymer Filled Rope: Rope in which the free internal spaces are filled with a solid polymer. The polymer extends to, or slightly beyond, the outer circumference of the rope.

Cushioned Rope: Stranded rope in which the inner layers, inner strands or core strands are covered with solid polymers or fibres to form a cushion between adjacent strands or layers of strands.

Cushion Core Rope: Stranded rope in which the core is covered (coated) or filled and covered (coated) with a solid polymer.

Solid Polymer Covered Rope: Rope which is covered (coated) with a solid polymer.

Solid Polymer Covered and Filled Rope: Rope which is covered (coated) and filled with a solid polymer.

Rope Grade (R.): A number corresponding to a wire tensile strength grade on which the minimum breaking force of a rope is calculated.

Note: It does not imply that the actual tensile strength grades of the wires in a rope are necessarily the same as the rope grade.

Preformed Rope: Stranded rope in which the wires in the strands and the strands in the rope have their internal stresses reduced resulting in a rope in which, after removal of any serving, the wires and the strands will not spring out of the rope formation.

Note: Multi-layer stranded ropes should be regarded as non-preformed rope even though the strands may have been partially (lightly) preformed during the closing process.

Rope Class: A grouping of rope constructions where the number of outer strands and the number of wires and how they are laid up are within defined limits, resulting in ropes within the class having similar strength and rotational properties.

Rope Construction: System which denotes the arrangement of the strands and wires within a rope, e.g. 6x36WS, 6x19S.

Note: K denotes compacted strands.

Cable-laid Rope: An assembly of several (usually six) single layer stranded ropes (referred to as unit ropes) laid helically over a core (usually a seventh single layer stranded rope).

Braided Rope: An assembly of several round strands braided in pairs.

Electro-mechanical Rope: A stranded or spiral rope containing electrical conductors.

#### Strand and Rope Lays

Lay direction of strand: The direction right (z) or left (s) corresponding to the direction of lay of the outer layer of wires in relation to the longitudinal axis of the strand.

Lay direction of rope: The direction right (Z) or left (S) corresponding to the direction of lay of the outer strands in relation to the longitudinal axis of a stranded rope or the direction of lay of the outer wires in relation to the longitudinal axis of a spiral rope.

Ordinary lay: Stranded rope in which the direction of lay of the wires in the outer strands is in the opposite direction to the lay of the outer strands in the rope. Right hand ordinary lay is designated sZ and left hand ordinary lay is designated zS.

Note: This type of lay is sometimes referred to as 'regular' lay.

Lang's lay: Stranded rope in which the direction of lay of the wires in the outer strands is the same as that of the outer strands in the rope. Right hand Lang's lay is designated zZ and left hand Lang's lay is designated sS.

Alternate lay: Stranded rope in which the lay of the outer strands is alternatively Lang's lay and ordinary lay. Right hand alternate lay is designated AZ and left hand alternate lay is designated AS.

Contra-lay: Rope in which at least one inner layer of wires in a spiral rope or one layer of strands in a stranded rope is laid in the opposite direction to the other layer(s) of wires or strands respectively.

Note: Contra-lay is only possible in spiral ropes having more than one layer of wires and in multi-layer stranded ropes.

Rope lay length (Stranded Rope): That distance parallel to the axis of the rope in which the outer strands make one complete turn (or helix) about the axis of the rope.

#### Cores

Core: Central element, usually of fibre or steel, of a single layer stranded rope, around which are laid helically the outer strands of a stranded rope or the outer unit ropes of a cable-laid rope.

Fibre core: Core made from natural fibres(e.g. hemp, sisal) and designated by its diameter and runnage.

Fibre Film Core: Core made from synthetic fibres (e.g. polypropylene) and designated by its diameter and runnage.

Steel core: Core produced either as an independent wire rope (IWRC)(e.g. 7x7) or wire strand (WSC)(e.g. 1x7).

Solid polymer core: Core produced as a single element of solid polymer having a round or grooved shape. It may also contain internal elements of wire or fibre.

Insert: Element of fibre or solid polymer so positioned as to separate adjacent strands or wires in the same or overlying layers and fill, or partly fill, some of the interstices in the rope. (see Zebra)

#### Rope Characteristics and Properties

Calculated Minimum aggregate Breaking Force: Value of minimum aggregate breaking force is obtained by calculation from the sum of the products of the cross-sectional area (based on nominal wire diameter) and tensile strength grade of each wire in the rope, as given in the manufacturer's rope design.

Calculated Minimum breaking Force: Value of minimum breaking force based on the nominal wire sizes, wire tensile strength grades and spinning loss factor for the rope class or construction as given in the manufacturer's rope design.

Fill factor: The ratio between the sum of the nominal crosssectional areas of all the load bearing wires in the rope and the circumscribed area of the rope based on its nominal diameter.

Spinning loss factor (k): The ratio between the calculated minimum breaking force of the rope and the calculated minimum aggregate breaking force of the rope.

Breaking force factor (K): An empirical factor used in the determination of minimum breaking force of a rope and obtained from the product of fill factor for the rope class or construction, spinning loss factor for the rope class or construction and the constant  $\pi/4$ .

# Conversion Factors S.I. Units

Force			
1 kN	= 0.101 972 Mp	1 UK tonf	= 9964.02N
1 N	= 0.101 972 kgf	1 lbf	= 4.448 22N
1 kgf	= 9.806 65 N	1 lbf	= 0.453 592 kgf
1 kgf	= 1 kp	1 UK tonf	= 1.01605 tonne
1 N	= 1.003 61 x 10 ⁻⁴ UK tonf	1 UK tonf	= 9.964 02 kN
1 N	= 0.2244 809 lbf	1 UK tonf	= 2240 lbf
1 kgf	= 2.204 62 lbf	1 short tonf	
1 t	= 0.984 207 UK tonf	(USA)	= 2000 lbf
1 kN	= 0.100 361 UK tonf	1 kip (USA)	= 1000 lbf
		1 kip	= 453.592 37 kgf
Pressure/	Stress		
1 N/mm ²	= 0.101972 kgf/mm ²		
1 kgf/mm	2	= 9.806 65 N/	mm ²
1 N/mm ²	= 1 MPa		
1 kgf/mm	2	= 1 422.33 lbf	/in ² 1 lbf/in ² =
7.031 x 10	D-4		
			kgf/mm ²
1 kgf/mm	2	= 0.634 971 to	onf/in ² 1 tonf/in ² =
1.574 88	kgf/mm²		
1 N/m ²	= 1.45038 x 10 ⁻⁴ lbf/in ²	1 lbf/in ²	= 6894 76 N/m ²
1 N/m ²	= 1 x 10 ⁻⁶ N/mm ²	1 tonf/in ²	= 1.544 43 x 10 ⁸
			dyn/cm ²
1 bar	= 14.503 8 lbf/in ²		

Minimum breaking force (Fmin): Specified value, in kN, below which the measured breaking force is not allowed to fall in a prescribed test and, for ropes having a grade, obtained by calculation from the product of the square of the nominal diameter, the rope grade and the breaking force factor.

Minimum aggregate breaking force (Fe,min): Specified value, in kN, below which the measured aggregate breaking force is not allowed to fall in a prescribed test and, for ropes having a grade, obtained from the product of the square of the nominal rope diameter (d), the metallic cross-sectional area factor (C) and the rope grade (Rr).

Nominal length mass: The nominal mass values are for the fully lubricated ropes. For friction winder ropes, the values should be reduced by 2%. The nominal length mass values are subject to a tolerance of plus 2% to minus 5%.

Rope torque: Value, usually expressed in N.m, resulting from either test or calculation, relating to the torque generated when both ends of the rope are fixed and the rope is subjected to tensile loading.

Rope turn: Value, usually expressed in degrees per metre, resulting from either test or calculation, relating to the amount of rotation when one end of the rope is free to rotate and the rope is subjected to tensile loading.

Initial extension: Amount of extension which is attributed to the initial bedding down of the wires within the strands and the strands within the rope due to tensile loading.

Note: This is sometimes referred to as constructional stretch.

Elastic extension: Amount of extension which follows Hooke's Law within certain limits due to application of a tensile load.

Permanent rope extension: Non-elastic extension.

Mass			
1 kg	= 2.204 62 lb	1 lb	= 0.453 592 kg
1 tonne (t)	= 0.984 207 UK ton	1 UK ton	= 1.01605 tonnes (t)
1 kg/m	= 0.671 970 lb/ft	1 lb/ft	= 1.488 kg/m
1 kg	= 1000 g	1 kip (USA)	= 1000 lb
1 Mp	= 1 x 10 ⁶ gf		
1 tonne (t)	= 9.80665 kN		
Length			
1 m	= 3.280 84 ft	1 ft	= 0.304 8 m
1 km	= 0.621 371 miles	1 mile	= 1.609 344 km
Area			
1 mm ²	= 0.001 55 in ²	1 in ²	= 645.16 mm ²
1 m ²	= 10.763 9ft ²	1 ft²	= 0.092 903 0 m ²
Volume			
1 cm ³	= 0.061 023 7 in ³	1 in ³	=16.387 1 cm ³
1 litre (1)	= 61.0374 in ³	1 in ³	= 1.6387 x 10 ⁴ ml
1 m ³	= 6.10237 x 10 ⁴ in ³	1 yd³	= 0.764 555 m ³

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